# Usporedba rotacijskih i recipročnih tehnika instrumentacije u mahaničkoj obradi zavijenih korijenskih kanala

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# COMPARISON OF ROTARY AND RECIPROCATING TECHNIQUES IN INSTRUMENTATION OF CURVED ROOT CANALS

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**Sažetak**

**USPOREDBA ROTACIJSKIH I RECIPROČNIH TEHNIKA INSTRUMENTACIJE U MEHANIČKOJ OBRADI ZAVIJENIH KORIJENSKIH KANALA**

Svrha doktorskog rada bila je usporediti transportaciju kanala i centričnost instrumenta u kanalu pet rotacijskih i recipročnih tehnika instrumentacije, različitih metalurškh svojstava i površinske obrade u zavijenim korijenskim kanalima. U ovom istraživanju korišteni su meziobukalni kanali 50 humanih izvađenih gornjih prvih i drugih molara. U svakoj skupini je slučajnim odabirom raspoređeno 10 uzoraka: Skupina 1: ProTaper Next (PTN); Skupina 2: Reciproc (RC); Skupina 3: Reciproc Blue (RCB); Skupina 4: TruNatomy (TRN); Skupina 5: XP-endo Shaper (XPS). Kanali su prije i tijekom instrumentacije ispirani s 5 ml 2,5% natrijevog hipoklorita (NaOCl). Nakon instrumentacije, korijenski kanali su završno isprani prema sljedećem protokolu: 15 % EDTA (1 min) i 2,5% NaOCl (30 s). Uzorci su skenirani u mikro-CT uređaju. Na mikro-CT snimkama prije i nakon instrumentacije korijenskih kanala softverski su izračunate udaljenosti ruba kanala od ruba korijena na udaljenostima 3, 5 i 7 mm od vrha korijena te je prema formulama izračunata transportacija kanala i centričnost instrumenta unutar kanala na navedenim razinama kanala. Za analizu rezultata korišten je jednosmjerni ANOVA test s odgovarajućim Post-hoc testom uz razinu značajnosti od 0,05. RCB je uzrokovao značajno veću kanalnu transportaciju u usporedbi s ostalim tehnikama ($p < 0,05$). Nije bilo statistički značajne razlike između ostalih skupina ($p > 0,05$). PTN je pokazao značajno bolju sposobnost da ostane centriran u korijenskom kanalu u usporedbi s RC i RCB tehnikama ($p = 0,046$, $p = 0,017$). U apikalnoj trećini kanala sve su tehnike pokazale sličnu kanalnu transportaciju i centričnost ($p > 0,05$). U srednjoj i cervikalnoj trećini kanala RCB je uzrokovao znatno veću transportaciju kanala nego ostale tehnike ($p < 0,05$). U ovom istraživanju sve ispitivane tehnike instrumentacije pokazale su slične vrijednosti kanalne transportacije i centričnosti instrumenta u apikalnom dijelu kanala. Ukupan rezultat, kao i rezultati u srednjem i koronarnom dijelu kanala ukazuju na to da uporaba recipročnih instrumenata rezultira većom transportacijom kanala i manjom centričnošću.

**Ključne riječi:** apikalna transportacija, centričnost intrumenta u kanalu, zavijeni korijenski kanali, mikrokompjuterizirana tomografija

**Summary**

**COMPARISON OF ROTARY AND RECIPROCATING TECHNIQUES IN THE INSTRUMENTATION OF CURVED ROOT CANALS**

**Aim:** The aim of this study was to evaluate the transportation and centering ability of 5 different rotary and reciprocating file systems with different metallurgical properties and surface treatments in curved root canals.

**Materials and methods:** Fifty mesiobuccal round canals of human upper first and second molars were assigned to 5 experimental groups (n = 10) according to the instrumentation system used: Group 1: ProTaper Next (PTN); Group 2: Reciproc (RC); Group 3: Reciproc Blue (RCB); Group 4: TruNatomy (TRN); Group 5: XP-endo Shaper (XPS). Before and during instrumentation, 5 mL 2.5% sodium hypochlorite (NaOCl) was used in each root canal. After instrumentation, the final irrigation protocol included 15 % EDTA (1 min) and 2,5% NaOCl (30 sec). The micro–computed tomographic scanning of the samples was performed before and after instrumentation to analyze the transportation and centering ability at three canal levels, 3, 5, and 7 mm from the apex. The results were analyzed by using the one-way analysis of variance test (ANOVA) with the corresponding post-hoc test.

**Results:** Overall, RCB caused significantly more canal transportation compared with the other techniques ($p < 0.05$). There were no significant differences between the other techniques ($p > 0.05$). ProTaper Next had a significantly better ability to stay within the central axis of the root canal compared with the Reciproc and RCB techniques ($p = 0.046$ and $p = 0.017$, respectively). In the apical third, all techniques caused similar apical transportation and centering ability ($p > 0.05$). In the middle and cervical parts of the canal, the RCB caused significantly greater canal transportation than the other techniques ($p < 0.05$).

**Conclusion:** Under the limitations of this study, all tested techniques had similar transportation and centering abilities in the apical part of the canal. However, the overall results and those in the middle and coronal parts of the canal indicated that reciprocating instruments resulted in more canal transportation and less centered preparations.

**Keywords:** Apical transportation, centering ability, curved root canals, micro–computed tomography

**SADRŽAJ**

**1. UVOD**……..…....1
1.1. Povijesni razvoj endodontskih instrumenata…….....…3
1.1.1. Razvoj strojnih endodontskih instrumenata po generacijama…….....……4
*1.1.1.1. Prva generacija endodontskih instrumenata*.....5
*1.1.1.2. Druga generacija endodontskih instrumenata*.....5
*1.1.1.3. Treća generacija endodontskih instrumenata*.....6
*1.1.1.4. Četvrta generacija endodontskih instrumenata*.....7
*1.1.1.5. Peta generacija endodontskih instrumenata*.....8
*1.1.1.6. Ekspandirajući instrumenti koji se prilagođavaju anatomiji kanala*…….....8
1.2. Nikal-titanski endodontski instrumenti……9
1.2.1. Mehaničko ponašanje Ni-Ti endodontskih instrumenata (metalurške karakteristike).....9
1.2.2. Superelastičnost Ni-Ti instrumenta.....10
1.2.3. Učinak tople sterilizacije na svojstva Ni-Ti instrumenata.....10
1.2.4. Pucanje NiTi instrumenata i mehanizmi pucanja.....11
*1.2.4.1. Torzijsko opterećenje, ciklički zamor i fleksibilnost instrumenta*.....11
1.2.5. Utjecaj mehaničke obrade kanala i ispiranja na intrakanalni dentin.....12
1.3. Rotacijske tehnike instrumentacije kanala.....13
1.3.1. ProTaper Next.....14
1.3.2. TruNatomy……..15
1. 4. Recipročne tehnike instrumentacije korijenskih kanala.....16
1.4.1. Recipročni pokret.....16
1.4.2. Povijesni razvoj recipročnih tehnika.....17
1.4.3. Reciproc tehnika instrumentacije.....19
1.4.4. Recipročni instrumenti s površinski obrađenom legurom Ni-Ti.....20
*1.4.4.1. Reciproc Blue*.....21
1.5. Iatrogene greške tijekom instrumentacije korijenskog kanala.....21
1.5.1. Transportacija korijenskog kanala.....21
1.5.2. Stepenica u korijenskom kanalu.....22
1.6. Sposobnost instrumenta da ostane centriran u kanalu tijekom instrumentacije.....23
1.7. Mjerenje stupnja zavijenosti korijenskog kanala zuba.....23
1.7.1. Mjerenje kuta za određivanje zavijenosti korijenskih kanala.....23
1.7.2. Određivanje zavijenosti korijenskih kanala metodom kuta i kružnica.....26

1.7.3. Računalno potpomognuto određivanje zavijenosti korijenskih kanala.....27
1.7.4.Trodimenzionalno određivanje zavijenosti korijenskih kanala.....27
1.8. Mikro-kompjuterizirana tomografija u endodontskim istraživanjima.....29

**2. CILJEVI I HIPOTEZE**.....31
**3. MATERIJALI I POSTUPCI**.....33
3.1. Odabir uzoraka za istraživanje.....34
3.2. Priprema uzoraka za istraživanje.....34
3.3. Mjerenje zavijenosti kanala mikro-komjuteriziranom tomografijom.....35
3.4. Instrumentacija korijenskih kanala.....38
3.5. Mikro-CT snimanje uzoraka.....44
3.6. Mjerenje transportacije kanala nakon instrumentacije.....45
3.7. Analiza centričnosti instrumenta u korijenskom kanalu .....47
3.8. Statistička analiza.....47

**4. REZULTATI**.....48
**5. RASPRAVA**.....63
**6. ZAKLJUČAK**.....72
**7. LITERATURA**.....74
**8. ŽIVOTOPIS**.....92

**Popis skraćenica**

| | |
|---|---|
| **ANOVA** | analiza varijance (eng. analysis of variance) |
| **CBCT** | Cone beam computed tomography |
| **CW** | engl. clock wise |
| **CCW** | engl. counterclock wise |
| **EDTA** | Etilendiamintetraoctena kiselina |
| **Mikro-CT** | Mikro-kompjuterizirana tomografija |
| **NaOCl** | Natrijev hipoklorit |
| **Ni – Ti** | Nikal – Ttitan |
| **Nitinol** | Nikal – Titan legura, „NOL“ – akronim Naval Ordinance Laboratorij |
| **PTN** | ProTaper Next |
| **RC** | Reciproc |
| **RCB** | Reciproc Blue |
| **SEM** | Skenirajuci elektronski mikroskop (engl. Scanning electron microscopy) |
| **TRN** | TruNatomy |
| **XPS** | XP-endo Shaper |

# 1. UVOD

Svrha je endodontskog liječenja ukloniti infekciju i iritanse (ostaci pulpnog tkiva, bakterijski biofilm, debris) iz kanalnog sustava zuba i spriječiti infekciju ili reinfekciju endodontskog prostora ili periradikularnog tkiva. To se postiže kemo-mehaničkom obradom korijenskog kanala, koja uključuje mehaničku instrumentaciju ručnim ili strojnim instrumentima i ispiranje različitim antimikrobnim sredstvima. Mehanička instrumentacija postupak je čišćenja, širenja i oblikovanja korijenskog kanala ručnim ili strojnim, čeličnim ili nikal-titanskim instrumentima. Svrha je širenja ukloniti inficirani dentin, olakšati ispiranje korijenskog kanala i osigurati prostor za postavljanje materijala za punjenje. Kriteriji kvalitetne instrumentacije korijenskog kanala jesu: izrada kanalnog sustava stalnog koniciteta, zadržavanje originalnog oblika kanala i položaja apikalnog otvora, glatki kanalni zidovi, oblikovanje apikalnog stopa (1). Zbog složene anatomije endodontskog prostora (istmusi, proširenja, lateralni i akcesorni kanali, ramifikacije) i radikularnog dentina ni ručnom ni strojnom instrumentacijom nije moguće u potpunosti očistiti korijenski kanal pa oko 35 % dentinskog zida i dalje ostaje neočišćeno i neinstrumentirano (2).

Danas na tržištu postoji preko 160 tehnika instrumentacije koje se međusobno razlikuju po poprečnom presjeku instrumenta, konicitetu, brojnosti reznih ploha, duljini, broju instrumenata u sekvenci i kinematici pokreta. Uspješnost pojedine tehnike ovisi o konstrukciji i dizajnu instrumenata, učinkovitosti oblikovanja kanala, uklanjanju inficiranog dentina i antimikrobnoj učinkovitosti (3, 4).

## 1.1. Povijesni razvoj endodontskih instrumenata

Stari Grci, Rimljani i Kinezi još 1500 godina prije Krista na razne su načine pokušavali spoznati i liječiti bol zuba. Postoje zapisi o stavljanju bakrene ili zlatne žice u korijenski kanal zuba kako bi se smanjila bol. Povijest endodontske terapije datira iz sredine 17. stoljeća kada je Charles Allen napisao prvu knjigu koja je bila posvećena samo zubima (5).

Prvi instrument za obradu korijenskog kanala radi ekstirpacije zubne pulpe predstavio je Edwin Maynard 1838. godine. Instrument je u početku izrađivan od opruge satnog mehanizma, kasnije od klavirske žice. Do 60-ih godina prošlog stoljeća koristili su se instrumenti izrađeni od čelika s udjelom ugljika. Njihov glavni nedostatak bila su loša fizikalna svojstva i korozija instrumenta uzrokovana sterilizacijom (6). Izradom instrumenata od nehrđajućeg čelika povećava se njegova rezna učinkovitost i otpornost na lom. Instrumenti od nehrđajućeg čelika sadržavaju 71 % željeza, 18 % kroma , 8 % nikla i manje od 0,2 % ugljika. Odlikuju se visokom krutošću, biokompatibilnošću i visokim modulom elastičnosti. Danas se najčešće upotrebljavaju K-instrumenti od nehrđajućeg čelika koje je 1915. godine predstavila tvrtka Kerr.

Godine 1960. William Bueller predstavlja nikal-titansku (Ni-Ti) leguru koja čini osnovu za razvoj suvremenih endodontskih instrumenata. Pojava Ni-Ti legura u endodonciji omogućila je kreiranje čvrstog instrumenta otpornog na koroziju s mogućnošću mehaničke memorije (7).

U izradi instrumenata razlikujemo strojnu i klasičnu tehniku. Strojna tehnika uključuje brušenje, odnosno tokarenje ili glodanje instrumenata izravno u tokarskom stroju. Svi Ni-Ti instrumenti izrađuju se na ovaj način, čime se povećava otpornost na lom. Klasična tehnika započinje brušenjem žice dok se ne postigne odgovarajući konicitet i presjek (kvadratičan, trokutast, romboidan). Zatim slijedi uvrtanje žice suprotno od smjera kazaljke na satu kako bi se dobio helikoidni rezni rub. S obzirom na konfiguraciju instrumenti su predviđeni za različite načine upotrebe (7, 8).

Standardizacija endodontskih instrumenata prvi je put objavljena 1976. godine kao specifikacija Američkog stomatološkog društva br. 28 (*American Dental Association, ADA, specification No. 28).* Prema navedenoj specifikaciji standardi se odnose isključivo na ručne instrumente, odnosno na njihov promjer, dužinu, otpornost na lom, čvrstoću i otpornost na koroziju (7).

Ručne tehnike obrade kanala zahtijevaju više vremena zbog nemogućnosti okretanja instrumenata za više od pola do cijelog okreta. Smatra se da je prijelaz na strojno vođenu endodontsku terapiju započeo Oltramare (9), koji je 1892. godine u upotrebu uveo iglu

četvrtastog presjeka koja se montirala u kolječnik. Prve strojne endodontske tehnike koristile su instrumente od nehrđajućeg čelika. Nedostatak čeličnih instrumenata mali je konicitet od 0,02. Naime oni tijekom instrumentacije velikom površinom dodiruju stijenke korijenskog kanala, što dovodi do izravnavanja zavijenih korijenskih kanala. To je potvrđeno u opsežnoj studiji tzv. Göttingen grupe (10). S obzirom na to da je kontaktna površina instrumenta i stijenki kanala velika, svaka dodatna rotacija instrumenta veća od 180° ili 360° znatno povećava mogućnost loma instrumenta. Ostali nedostaci odnose se na velike nakupine zaostalog debrisa i zaostatnog sloja (11, 12), kao i na blokadu apeksnog otvora, perforacije kanala i gubitak radne duljine (13). Godine 1889. William H. Rollins (14) razvio je prvi kolječnik namijenjen automatskoj obradi korijenskog kanala koristeći specijalno dizajnirane rotirajuće instrumente. Brzina tih instrumenata bila je ograničena na 100 okretaja u minuti. Kombinirana kretnja rotacije i vertikalna kretnja instrumenata prvi su put opisane i stroj je prvi put izrađen u austrijskoj kompaniji W&H (Burmoos, Austrija) 1928. godine (10). Strojna endodoncija postaje popularna razvojem sustava Giromatic u Francuskoj (MicroMega, Besançon) 1964. godine. Smatra se da je Giromatic prethodnik recipročne tehnike jer je i sam stroj radio recipročni pokret od 90° ulijevo i udesno. Svi instrumenti u tom periodu bili su izrađeni od čelika, a stomatolozi su mogli kontrolirati samo brzinu okretaja i ručno promijeniti amplitudu pomaka instrumenta (10).

Danas razlikujemo sustave koji koriste rotacijske kretnje, recipročne kretnje, njihovu kombinaciju (adaptivni sustavi) te vibracijske kretnje (ultrazvučne i zvučne te tzv. *push and pull motion* tehnike).

### 1.1.1. Razvoj strojnih endodontskih instrumenata po generacijama

Razvojem metalurgije i kliničkim te znanstvenim naporima stomatološke zajednice razvijene su i u stalnoj kliničkoj uporabi prisutne brojne strojne tehnike instrumentacije. Do danas je opisano pet generacija Ni-Ti instrumenata s obzirom na njihov kronološki slijed pojavljivanja na tržištu, karakteristike i način primjene u korijenskom kanalu.

*1.1.1.1. Prva generacija endodontskih instrumenata*

**Prva generacija** strojnih instrumenata pojavila se 1992. godine kada je John McSpadden dizajnirao prvi rotirajući strojni instrument koniciteta 0,02 (3). Iako su unijeli velike promjene u instrumentaciji korijenskih kanala, lom instrumenta i dalje je predstavljao problem. Dvije godine poslije Ben Johnson mijenja paradigmu ISO 0,02 koniciteta instrumenata i uvodi instrumentacijski sustav ProFile s instrumentima koniciteta od 0,04 i 0,06 te instrumentima za oblikovanje ulaza u korijenske kanale (tzv. *orifice shapers*). Johnsonove instrumente odlikuje klasični dizajn s utorima, čime je smanjena mogućnost urezivanja instrumenta u dentin korijenskog kanala, a dentin se reže pasivnim struganjem. Johnson i McSpadden smatraju se očevima Ni-Ti rotirajućih instrumenata.
Ubrzo nakon toga razvijeni su i drugi rotirajući sustavi kao što su LightSpeed (Light Speed Technology Inc, San Antonio, Teksas, SAD; Senia i Wildey), Quantec (Tycom, Irvine, Kalifornija, SAD; McSpadden) i Greater Taper (Tulsa Dental Products, Tulsa, Oklahoma, SAD; Buchanan) (15).

Zajedničko svojstvo svim sustavima prve generacije pasivan je rezni brid i stalni konicitet čitavom radnom dužinom instrumenta. To osigurava centriranost instrumenta u kanalu i sprečava njegovo vezanje za stijenke kanala, ali povećava lateralnu rezistenciju na stijenkama kanala, koja pri povećanom okretnom momentu dovodi do loma instrumenta. Još jedna negativna karakteristika ovih sustava jest i uporaba velikog broja različitih instrumenata.

*1.1.1.2. Druga generacija endodontskih instrumenata*

**Druga generacija** Ni-Ti rotacijskih instrumenata pojavila se na tržištu krajem 90-ih godina 20. stoljeća. Od prethodne generacije razlikuju se po konicitetu koji se povećava i smanjuje duž radnog dijela instrumenta te aktivnom reznom bridu. Kut između reznog brida i uzdužne osi instrumenta manji je nego u prvoj generaciji, što uvelike smanjuje uvrtanje i uklještenje instrumenta (engl. *screwing effect*) (1, 5). Tu pripadaju sustavi: ProTaper (Dentsply-Maillefer, Ballaigues, Švicarska), K3 (Sybron Endo, Orange, CA), M-Two (Dentsply-Maillefer, Ballaigues, Švicarska). Smanjen je i broj instrumenata potrebnih za obradu kanala.
ProTaper instrumenti imaju promjenjiv konicitet, tj. smjenjuju se različiti koniciteti na pojedinom instrumentu. Izvorno se sastoji od šest instrumenata: tri instrumenta za oblikovanje korijenskih kanala (engl. *shaping files*) i tri završna instrumenta (engl. *finishing files*).

Neki instrumenti druge generacije, primjerice sustav K3 (SybronEndo, Orange, CA), dizajnirani su s pozitivnim kutom nagiba (engl. *rake angle*), što je omogućilo učinkovitije rezanje dentina (engl. *cutting efficiency*). Da bi se smanjilo urezivanje instrumenta u stijenke dentina korijenskih kanala (engl. *taper lock*), predstavljeni su novi instrumenti EndoSequence (Brasseler, Savannah, GA, SAD) i BioRaCe (FKG Dentaire, La Chaux-de-Fonds, Švicarska), koji imaju promjenjiva kontaktna mjesta/površine instrumenta i dentina. Ova karakteristika smanjuje urezivanje i zaglavljivanje instrumenta. Instrument još uvijek ima stalan konicitet u aktivnom dijelu (16).

Instrumenti BioRaCe (FKG Dentaire, La Chaux-de-Fonds, Švicarska) u svojoj završnoj fazi proizvodnje podliježu elektropoliranju radi smanjenja površinskih defekata i poboljšanja mehaničkih svojstava instrumenta (17). Otpornost na zamor materijala, tj. instrumenta ovisi o izgledu površine Ni-Ti instrumenata jer je najviše „pogrešaka instrumentacije" povezano sa zamorom materijala. Da bi se poboljšala svojstva Ni-Ti instrumenata, otpornost na ciklički zamor i učinkovitost uklanjanja dentina, razvijeni su novi postupci u proizvodnji uključujući implementaciju iona (18 - 20) i elektropoliranje (21 - 23) površine instrumenta.

### *1.1.1.3. Treća generacija endodontskih instrumenata*

Napredak u metalurgiji Ni-Ti obilježio je nastanak **treće generacije** instrumenata. Instrumenti su podvrgnuti posebnoj vrsti toplinske obrade kako bi se povećala otpornost materijala na lom, zamor i osigurala učinkovitija upotreba instrumenata (2, 5). Tu pripadaju sustavi: Hyflex CM (HyFlex, Coltene Whaledent, Cuyahoga Falls, OH), K3XF (SybronEndo, Orange, CA), ProFile GT Series X (GTX; Dentsply Tulsa Dental Specialties, Tulsa, OK), ProFile Vortex (Dentsply Tulsa Dental, Tulsa, OK), Vortex Blue (Dentsply Tulsa Dental, Tulsa, OK), Typhoon (TYP; Clinician's Choice Dental Products, New Milford, CT) i Twisted files (SybronEndo, Orange, CA).

Serijom toplinske obrade Ni-Ti žice dobivena je M-wire (Sportswire, Langley, OK) Ni-Ti legura koja je na tržištu predstavljena 2007. godine. Završna je temperatura austenita M-žice (engl. *M-wire*) 43 °C – 50 °C (24 - 28). Time je znatno iznad završne temperature konvencionalnog Ni-Ti i tjelesne temperature. To znači da se M-žica ne sastoji samo od austenita u kliničkim uvjetima. Mnogobrojna istraživanja pokazala su da M-žica na tjelesnoj temperaturi sadrži austenitnu fazu i mali udio martenzitne i R-faze (24, 26, 27). Iz tog razloga M-žica održava superelastično stanje (29) i pokazuje veću fleksibilnost u odnosu na konvencionalno proizvedenu Ni-Ti žicu. Poznato je da je modul elastičnosti martenzita i R-faze

niži nego austenita. Dijagram naprezanja pokazuje da je potrebno manje naprezanja da bi se inducirala martenzična transformacija M-žice nego konvencionalnog Ni-Ti. Još jedna značajna prednost M-žice jest veća otpornost na ciklički zamor. Predstavnici ove skupine jesu instrumenti ProFile GT Series X (GTX; Dentsply Tulsa Dental Specialties, Tulsa, OK), ProFile Vortex (Dentsply Tulsa Specialties, Tulsa, OK), Vortex Blue (Dentsply Tulsa Specialties, Tulsa, OK).

Posebnim termomehaničkim procesima koji kontroliraju memoriju materijala dobivena je nova legura Ni-Ti, tzv. CM žica (engl. *CM wire, controlled memory wire).*

CM žica izuzetno je fleksibilna, ali ne posjeduje memoriju oblika kao ostali Ni-Ti instrumenti. Predstavnici ove skupine jesu sustavi Hyflex CM (HyFlex, Coltene Whaledent, Cuyahoga Falls, OH) i Typhoon CM (Clinician's Choice Dental Products, New Milford, 2CT). Ovi instrumenti imaju manji udio nikla (52 %) nego konvencionalni Ni-Ti instrumenti (54,5 - 57 %).

Godine 2008. Sybron Endo predstavio je prvi Ni-Ti instrument s navojima dobiven plastičnom deformacijom. Proces je sličan procesu uvrtanja kojim se dobiva većina instrumenata od nehrđajućeg čelika. Prema proizvođaču toplinska obrada omogućava uvrtanje žice tijekom fazne transformacije u tzv. R-fazu Ni-Ti. Instrument je u početku bio dostupan samo u veličini 25 i konicitetu 0,04 do 0,12. Kasnije su dodane veličine 30, 35 i 40 (5).

### *1.1.1.4. Četvrta generacija endodontskih instrumenata*

**Četvrta generacija** obuhvaća instrumente koji koriste recipročnu kretnju pri obradi korijenskih kanala. Blanc, francuski stomatolog, još je 1950. godine predstavio recipročnu kretnju kao bilo koju ponavljajuću kretnju koja uključuje pokrete naprijed-natrag i gore-dolje. U početku su svi motori za recipročnu kretnju i pripadajući instrumenti koristili rotirajuću kretnju pod kutom od 90º u smjeru kretanja kazaljke na satu (engl. *clockwise, CW*) i suprotno od smjera kretanja kazaljke na satu (engl. *counterclockwise, CCW*).

Koncept jednog instrumenta razvio je kanadsko-libanonski znanstvenik i kliničar Ghassan Yared 2008. godine (30, 31). U izvornoj tehnici korišten je samo jedan ručni, čelični instrument (0,08) i apeks lokator. Nakon što je postignuta prohodnost kanala i određena radna duljina (engl. *working length, WL*), korišten je jedan F2 ProTaper Ni-Ti instrument (Tulsa Dentsply, Tulsa, OK, SAD). Instrument je korišten u kolječniku s motorom ATR Vision (ATR, Pistoia, Italija) s mogućnošću recipročnog pokreta (redukcija 16 : 1) u smjeru kazaljke na satu (CW) i u smjeru suprotnom od smjera kazaljke na satu (CCW). Instrument je pomican u kanalu

tzv. pakirajućim pokretima uz ekstremno male sile tlačenja prema apeksu uz često čišćenje i ispiranje otopinom natrijeva hipoklorita. Budući da instrument F2 ProTaper nije primarno razvijen za recipročnu kretnju, u trenutku CW kretnje je zarezao dentin, a CCW kretnja je oslobađala instrument. CW kretnja bila je duža od CCW kretnje pa se tako oblikovao konicitet kanala. Osim toga kombinacija CW i CCW kretnje, teoretski, smanjuje incidenciju torzijskog loma instrumenta. Yared (30) navodi da je u to doba prednost nove tehnike bila i u tome što nije zahtijevala predtretman kanala ručnim instrumentima do broja #15 ili #20 čak i kod jako zavijenih kanala. Brzo je ispravljena činjenica da je u recipročnoj tehnici korišten instrument zapravo konstruiran za konvencionalnu, rotacijsku tehniku pa su konstruirani novi, namjenski instrumenti: Wave One (Dentsply Sirona, Salzburg, Austrija) i Reciproc (VDW, München, Njemačka) (2). Oba instrumenta izrađena su od M-žice.

#### *1.1.1.5. Peta generacija endodontskih instrumenata*

**Peta generacija** instrumenata iskorištava gibanje vala duž aktivnog dijela instrumenta, što je moguće zbog pomaknutog centra rotacije, koji prenosi mehaničku rotaciju u gibanje valova (1). Takav dizajn smanjuje povezanost između instrumenta i dentina prevenirajući lom instrumenta. Sustavi koji koriste ovaj način rada jesu: Revo S (Micro-Mega®, Besançon, Francuska), One Shape (Micro-Mega®, Besançon, Francuska) i ProTaper Next (Dentsply Tulsa Dental Specialties, Johnson City, Tennessee, SAD/ Dentsply Maillefer, Ballaigues, Švicarska ).

#### *1.1.1.6. Ekspandirajući instrumenti koji se prilagođavaju anatomiji kanala*

Novi pristup u dizajnu i vrsti kretnje predstavlja **Self Adjusting File** (SAF; ReDent-Nova, Raana, Izrael). Instrument izgleda kao šuplji cilindar, a izrađen je od Ni-Ti rešetke abrazivne površine koja omogućava simultanu irigaciju tijekom mehaničke obrade korijenskog kanala. Kada je u kanalu, SAF ima sposobnost prilagodbe obliku kanala.

**XP-endo Shaper** (XPS; FKG, La Chaux-de-Fonds, Švicarska) novi je *single file* sustav čiji su instrumenti proizvedeni od Ni-Ti MaxWire legure. Ova legura dozvoljava kontrakciju i širenje instrumenta pa on tako doseže sve površine kanala. XPS se transformira iz martenzične u austenitnu fazu kada je u kanalu (na 37 °C). Ova metalurška promjena legure smanjuje rizik torzijskog i cikličkog zamora te poboljšava sposobnost oblikovanja kanala (15). Vršak instrumenta (engl. *booster tip*) sastoji se od šest reznih bridova koji omogućuju postepeno oblikovanje kanala, ISO veličine od 15 do 30, održavajući instrument centriranim u kanalu i

izbjegavajući izravnavanje kanala. Prema našim saznanjima malo je istraživanja koja su se bavila sposobnošću XPS-a da oblikuje korijenski kanal i održi njegovu izvornu anatomiju uz minimalnu kanalnu transportaciju (32, 33).

## 1.2. Nikal-titanski endodontski instrumenti

Leguru Ni-Ti, kakva se danas koristi za izradu endodontskih instrumenata, razvio je Bühler sa suradnicima. Ime legure, Nitinol, dolazi od nikal, titan i naziva laboratorija u kojem je proizvedena - Naval Ordnance Laboratory. Legura se sastoji od 55 % nikla i 45 % titana. Pokazuje superelastična svojstva i ima memoriju oblika uz određene uvjete proizvodnje (34).

### 1.2.1. Mehaničko ponašanje Ni-Ti endodontskih instrumenata (metalurške karakteristike)

Leguru nikla i titana (Ni-Ti) nazivamo i materijalom s memorijom jer se i nakon deformacije vraća u prvobitan položaj (2, 5). Ni-Ti instrumenti elastičniji su od čeličnih instrumenata i omogućavaju lakši ulazak u uske i zakrivljene dijelove kanala te prate njegov prirodan tijek s manjom učestalosti transportacije (2, 6, 7). Međutim zbog velike elastičnosti Ni-Ti instrumenti ne mogu se preoblikovati savijanjem prije uvođenja u kanal (8). Mehaničko ponašanje superelastičnih, nesuperelastičnih i legura Ni-Ti s memorijom oblika proizlazi iz prirode i udjela njihovih mikrostrukturnih faza. Za njihova svojstva zadužene su tri faze Ni-Ti legure: austenitna, martenzična i R – faza (34).

Austenit odlikuje kubična struktura kristalne rešetke, visoke temperature i manje naprezanje.

Martenzit ima monoklinsku strukturu kristalne rešetke, prisutan je na nižim temperaturama i pri većim naprezanjima. Transformacija iz austenita u martenzit događa se na nivou atoma. Memorija oblika proizlazi iz reverzibilnosti ovog procesa (35).

Romboedarski iskrivljena R-faza javlja se prilikom prelaska iz martenzita u austenit pri zagrijavanju i obrnuto (austenita u martenzit) pri hlađenju (14). Nastanku R-faze pogoduje prisutnost dislokacija i precipitata u leguri Ni-Ti, koji nastaju tijekom procesa proizvodnje.

Martenzit pokazuje niži modul elastičnosti (oko 30 - 40 GPa) od austenita (oko 80 - 90 GPa), a modul elastičnosti R-faze još je niži od onog kod martenzita (15). Ako je temperatura iznad završne temperature austenita, legura je u austenitnom stanju, tj. kruta, tvrda i posjeduje vrhunska **superelastična svojstva**. Ako je temperatura ispod završne temperature martenzita,

Ni-Ti legura u martenzičnom je stanju, meka, vodljiva, lako se može deformirati i ima **sposobnost memorije** (16).

Za faznu transformaciju bitne su sljedeće vrijednosti: As početna temperatura austenične transformacije, Af završna temperatura austenita, Ms početna temperatura martenzične transformacije, Mf završna temperatura martenzita, Rs početna temperatura R-faze i Rf završna temperatura R-faze. Kada se Ni-Ti instrument ohladi na dovoljno nisku temperaturu, sastoji se samo od martenzita. Pri zagrijavanju martenzit se počinje transformirati u R-fazu, daljnjim zagrijavanjem R-faza počinje prelaziti u austenit. Transformacija završava na Af temperaturi. Ako se endodontski instrument dalje zagrijava preko završne temperature austenita, sastojat će se u potpunosti samo od austenitne faze.

### 1.2.2. Superelastičnost Ni-Ti instrumenta

Superelastičnost Ni-Ti endodontskih instrumenata svojstvo je koje omogućava da se instrument vrati u svoj prvobitan oblik nakon deformacije, što ih razlikuje od nehrđajućih čeličnih instrumenata koji podliježu trajnoj deformaciji i promjeni oblika. Ovo svojstvo osiguralo je Ni-Ti endodontskim instrumentima veću fleksibilnost i mogućnost bolje prilagodbe instrumenta u zavijenim korijenskim kanalima, veću otpornost na lom i trošenje u usporedbi s instrumentima od nehrđajućeg čelika (34).

Legure Ni-Ti koje pokazuju svojstvo superelastičnosti podliježu transformaciji austenita u martenzit (tzv. martenzična transformacija) uzrokovanoj naprezanjem ili promjenom temperature. Prestankom naprezanja instrument se vraća u fazu austenita, tj. u prvobitan oblik. Ove legure mogu podnijeti do 10 % naprezanja i potpuno se oporaviti, za razliku od konvencionalnih legura koje podnose najviše 1 % naprezanja (34, 36).

### 1.2.3. Učinak tople sterilizacije na svojstva Ni-Ti instrumenata

Topla sterilizacija najčešće je korištena metoda za sterilizaciju instrumenata u stomatologiji. Ova metoda podrazumijeva sterilizaciju u autoklavu na temperaturi od 134 °C, uz tlak od 30 psi (37).

Topla sterilizacija može uzrokovati promjene u fizikalnim i mehaničkim svojstvima stomatoloških instrumenata. Ove promjene pogađaju vanjsku površinu instrumenta i pojavljuju se kao mikropukotine i korozivne promjene (38), smanjuju reznu učinkovitost, mijenjaju

otpornost instrumenta na ciklički ili torzijski zamor (39). Otkriveno je da ponovljena topla sterilizacija izaziva promjene u torziji, savitljivosti instrumenata (40, 41) i reznoj učinkovitosti (42, 43). Topla sterilizacija dovodi do oporavka oblika deformiranih instrumenata. Dvije trećine deformiranih instrumenata potpuno se vrate u stari oblik nakon sterilizacije (44). Istraživanja iz 2018. proučavala su utjecaj tople sterilizacije na otpornost na ciklički zamor Ni-Ti instrumenata proizvedenih termomehaničkim postupcima. Pedulla et al. (45) zaključili su da ponovljena topla sterilizacija ne utječe na ciklički zamor Ni-Ti instrumenata.

### 1.2.4. Pucanje Ni-Ti instrumenata i mehanizmi pucanja

U procesu proizvodnje Ni-Ti instrumenata nastaju brojni površinski defekti. Nepravilnosti na površini instrumenta kao što su žljebovi, mikropukotine i debris mogu se otkriti preglednom elektronskom mikroskopijom (engl. *scanning electron microscopy, SEM*) na površini novih, tvorničkih instrumenata (34). Više površinskih nepravilnosti primijećeno je kod instrumenata većeg koniciteta, što je rezultat složenijeg procesa proizvodnje (46). Kao rezultat takvih tvorničkih oštećenja jedan od mehanizama pucanja instrumenta mogao bi biti širenje tvornički nastalih utora na instrumentu uslijed odlaganja dentinskog debrisa tijekom instrumentacije (47). Neizvjesno je utječe li brzina okretanja instrumenta u kanalu na lom instrumenta. Endodontski motori s niskim snagama okretaja (engl. *torque*) ograničavaju oštećenje instrumenta u kanalu i smanjuju ciklički zamor instrumenta (48). S druge strane Beruti i suradnici (49) smatraju da su rotacijski Ni-Ti sustavi učinkovitiji pri većim snagama okretaja, a da rad pri niskim snagama okretaja uz upaljenu funkciju *auto-reverse* može rezultirati nepotrebnim nakupljanjem stresa i smanjenom trajnosti instrumenta.
Jedan od predisponiranih faktora za pucanje instrumenta je i konfiguracija kanala. U zavijenim kanalima, na mjestu najveće zakrivljenosti, najveći je ciklički zamor instrumenta, što može uzrokovati lom (50, 51). Instrumentacija u složenom kanalnom sustavu može dovesti do torzijskog opterećenja i pucanja instrumenta (52 - 54).

#### *1.2.4.1. Torzijsko opterećenje, ciklički zamor i fleksibilnost instrumenta*

Ni-Ti instrumenti su dva do tri puta fleksibilniji i otporniji na torzijsko pucanje od instrumenata od nehrđajućeg čelika (55). Međutim zbog niske granice razvlačenja (engl. *yield strength*) i niske vlačne čvrstoće osjetljiviji su na pucanje pri manjim opterećenjima (56). Znakovi oštećenja instrumenta vidljiviji su kod ručnih instrumenata od nehrđajućeg čelika nego kod

strojnih Ni-Ti instrumenata (57) pa se za Ni-Ti instrumente često kaže da pucaju bez upozorenja (58).

Ni-Ti instrumenti pucaju zbog cikličkog ili torzijskog zamora ili kombinacije obaju (59). Ponovljeno naprezanje instrumenta tijekom uporabe uzrokuje ponovljene transformacije legure iz austenita u martenzit, što uzrokuje promjene mehaničkih svojstava instrumenta.

Do frakture instrumenta uzrokovane torzijskim opterećenjem dolazi kada se instrument (preciznije vršak instrumenta) zaglavi u dentinu kanala, a ostatak instrumenta nastavi se rotirati pa isti puca zbog plastične deformacije koja se manifestira kao odmotavanje navoja, ispravljanje ili *twisting* instrumenta (60).

Ciklički zamor instrumenta događa se pri kontinuiranim rotacijama instrumenta u zavijenim korijenskim kanalima stvarajući tenzijske/tlačne cikluse na mjestu najveće zakrivljenosti, što rezultira pucanjem instrumenta (60, 61).

Prema nekim istraživanjima većina se fraktura događa zbog fleksijskog zamora (engl. *flexural fatigue*) koji je posljedica prekomjerne uporabe metalne legure (62 - 64). Ostali su faktori, koji potencijalno doprinose zamoru legure, korozija i promjene uzrokovane toplinskom ekspanzijom i kontrakcijom (65). Drugi autori navode da je torzijska fraktura dominantan način pucanja instrumenta. Uzrokovana je prekomjernom apikalnom silom tijekom instrumentacije ili kompleksnom anatomijom zuba (velika zavijenost korijenskih kanala) (66).

U pravilu, torzijsko pucanje opada, a fleksijsko raste s rastom veličine instrumenta (67).

### 1.2.5. Utjecaj mehaničke obrade kanala i ispiranja na intrakanalni dentin

Liječenje korijenskih kanala obuhvaća mehaničke i kemijske postupke koji oslabljuju strukturu zuba. Gubitak marginalnog ruba, uklanjanje krova pulpne komore, proširivanje ulaza u korijenske kanale i instrumentacija korijenskih kanala, uporaba otopina za dezinfekciju i intrakanalnih uložaka, odabir punila i tehnike punjenja i u konačnici tip koronarne restauracije formiraju lanac terapijskih postupaka koji imaju kumulativni učinak na preostali intrakanalni dentin i njegova kemijska i fizička svojstva (68). Pokazatelji ovog utjecaja jesu: odnos instrumentirane i neinstrumentirane površine dentina, promjene površinske strukture, znakovi instrumentacije (engl. *preparation marks*), ostaci metala (engl. *metal deposits)* (male količine željeza, nikla, aluminija i titanija) (69), hrapavost/glatkoća dentina, mikročvrstoća, demineralizacija, erozija, zaostatni sloj (engl. *smear layer*) / otvoreni dentinski tubulusi, propusnost dentina, otpornost na frakturu, promjene temperature, snaga veze dentina s adhezivima i punilima, diskoloracije i kumulativni efekt.

Rezanje dentina endodontskim instrumentima od nehrđajućeg čelika ili Ni-Ti uzrokuje stvaranje zaostatnog sloja (engl. *smear layer*). Zaostatni sloj sastoji se od čestica dentina, ostataka vitalnog ili nekrotičnog pulpnog tkiva, bakterija i zaostalog irigansa (70). Debljina zaostatnog sloja je od 1 do 5 μm, a može se proširiti i na dentinske tubuluse do 49 μm (71).
Zaostatni sloj smanjuje permeabilnost dentina i snagu veze dentina s adhezivima i punilima te sprečava prodiranje irigansa u dublje slojeve intrakanalnog dentina.
Istraživanja su pokazala da se zaostatni sloj može učinkovito ukloniti samo uz pomoć kiselina i kelatora ili ultrazvučno (70 - 72).
Mehanički pokreti endodontskih instrumenata mogu ozbiljno narušiti integritet korijena zuba stvarajući mikropukotine (engl. *microcracks*), nepotpune frakturne linije (engl. *craze lines*), nepravilnosti površine dentina i potpune frakture korijena. Pukotine u dentinu ili fraktura korijena nastaju kada vlačno naprezanje na zidu korijenskog kanala premaši vlačno naprezanje dentina (73).
U novije vrijeme dizajnirani su instrumenti različitih kutova i oblika vrha kako bi se smanjile greške tijekom preparacije. Naime instrument može stvoriti „lažni kanal" ne prateći originalnu zakrivljenost kanala, čime u konačnici može doći i do perforacija.

### 1.3. Rotacijske tehnike instrumentacije kanala

William H. Rollins razvio je prvi sustav za strojnu instrumentaciju korijenskih kanala 1889. godine. Sustav se sastojao od posebno oblikovanih instrumenata koji su se rotirali za 360 stupnjeva brzinom od 100 okretaja u minuti (14). Svi kasnije proizvedeni Ni-Ti rotacijski sustavi uglavnom slijede iste mehaničke principe te se rotiraju za 360 stupnjeva uz nešto veći ali ipak relativno nizak broj okretaja.

Rotacijski Ni-Ti instrumenti mogu imati režući ili nerežući vrh, pri čemu ih režući vrh čini puno agresivnijima. Prednost instrumenata s režućim vrhom sposobnost je probijanja kalcificiranih kanala, ali je veća vjerojatnost stvaranja stepenice ili perforacije stijenke korijenskih kanala. Još jedna važna značajka instrumenta njegov je konicitet (engl. *taper*). Na tržištu postoje instrumenti s jednakim konicitetom duž radnog dijela ali s različitim promjerom vrška instrumenta i instrumenti koji imaju promjenjiv konicitet koji varira od 0,04 do 0,012 (74). Kod instrumenata s promjenjivim konicitetom smanjuje se trenje i potreban je manji okretni moment (engl. *torque*) za instrumentaciju. Na reznu učinkovitost instrumenata utječe i kut nagiba (engl. *rake angle*). To je kut između reznog brida i poprečnog presjeka okomito na dužinsku os

instrumenta. Učinkovitiji su instrumenti s pozitivnim kutom nagiba, no pretjerano pozitivan kut nagiba rezultira „kopanjem" dentina i mogućim lomom instrumenta. Većina instrumenata dolazi s negativnim ili uglavnom neutralnim kutom nagiba. Primjerice instrumenti ProFile imaju negativan kut nagiba, dok K3, ProTaper, Hero 642, RaCe i Flex Master sustavi imaju pozitivan kut nagiba, što rezultira optimalnom reznom učinkovitošću (75). Još jedna važna značajka instrumenata jesu radijalne površine. To je površina koja prolazi aksijalno od središnje osi, između žljebova, do reznog ruba. Što je ta površina manja, to je otpornost na naprezanje instrumenta, uzrokovana rotacijom ili uvijanjem, manja (76). Kombinacija nerežućeg vrha i radijalne površine utječe na centriranost instrumenta unutar korijenskog kanala. Prije su rotirajući instrumenti imali potpune radijalne površine (Profile, GT) ili su one bile udubljene (Quantec). ProTaper, Hero 642, Endo Sequence (Brasseler, Ventura, SAD) i RaCe nemaju radijalne površine.

Varijabilni spiralni kut (engl. *helical flute angles*) još je jedno od svojstava koje utječe na učinkovitost rotacijskih instrumenata. Spiralni kut jest kut koji rezni bridovi zatvaraju s dužinskom osi instrumenta. Rastom spiralnog kuta od vrha prema ručki poboljšava se uklanjanje dentinskih ostataka iz kanala (5, 76).

Potrebno je brzo i učinkovito uklanjanje debrisa prilikom instrumentacije korijenskih kanala, a instrumenti koji imaju nepromjenjiv spiralni kut uzrokuju nakupljanje debrisa i skloniji su stvaranju učinka „šarafljenja". RaCe instrumenti jedinstveni su po svom promjenjivom spiralnom dizajnu koji omogućuje manji okretni zamor prilikom rotacije izmjenom spiralnih i ravnih dijelova duž radne duljine instrumenta (77).

### 1.3.1. ProTaper Next

ProTaper Next jedna je od najčešće korištenih rotacijskih tehnika instrumentacije koja je naslijedila ProTaper Universal. S prethodnim sustavom, osim naziva, nema mnogo sličnosti. Temelji se na ideji „vijugajućih instrumenata" dr. M. Scianambloa iz SAD-a (engl. „swaggering effect").

Ovi instrumenti imaju simetričan pravokutni poprečni presjek koji je u odnosu na rotacijsku os pomaknut, tzv. „ off set design", tako da se os središta mase vijuga oko osi rotacije instrumenta, slično lentulo-spirali. Kao rezultat nastaje instrument koji ima mnogo više prostora za rezanje dentina uz veću učinkovitost rezanja, veću fleksibilnost, manji moment opterećenja tijekom

instrumentacije, veći otpor na lom, mnogo lakše vođenje i bolji taktilni osjećaj (78). Omogućava bolje centriranje instrumenta u kanalu i posljedično očuvanje izvorne anatomije kanala (79, 80)

Zahvaljujući spiralnom obliku instrument, u slučaju djelovanja prejake sile, djeluje kao opruga: višak sile pohranjuje i nakon rasterećenja iskorištava za oblikovanje kanala. Slično ručnoj *balanced force* tehnici po Roaneu sile se uravnotežuju. Glavna mu je karakteristika različita koničnost duž radnog dijela i pravokutni poprečni presjek koji tijekom rada dodiruje stijenke kanala samo u dvjema točkama. Posjeduje jedinstven dizajn s ekscentričnim stupnjem rotacije, poboljšavajući obradu i instrumentaciju korijenskog kanala (79). Klinički, ovako konstruiran instrument pridonosi smanjenju uglavljivanja vrha instrumenta u stijenke kanala tijekom rada, povećavajući prostor za rezanje i odlaganje detritusa. Proizvodi se od M- žice, što mu povećava fleksibilnost i otpornost na ciklički zamor (81).

Sustav se sastoji od pet instrumenata: X1 (17/04), X2 (25/06) te X3 (30/05), X4 (40/05) i X5 (50/06) u tri duljine (21 mm, 25 mm i 31 mm) od kojih obično nakon osiguravanja prohodnosti koriste samo dva do tri.

### 1.3.2. TruNatomy

**TruNatomy (TRN) (Dentsply Sirona, Ballaigues, Švicarska)** nedavno je predstavljen rotacijski sustav, dizajniran da se prilagođava kanalu i prati njegovu anatomiju. Instrumenti su izrađeni od 0,8 mm debele Ni-Ti žice koja podliježe posebnoj toplinskoj obradi, što osigurava superelastična svojstva instrumenata i manje memorije oblika u usporedbi s konvencionalnom M-žicom. Instrumenti imaju regresivni konicitet i *off–centered* poprečni presjek, što znači da instrument asimetrično radi u kanalu. TRN omogućava instrumentaciju uskih i zavijenih kanala uz očuvanje integriteta zuba, uklanjajući dentin samo gdje je klinički potrebno. S obzirom na to da svi instrumenti imaju isti koronarni promjer, ne dolazi do nepotrebnog proširivanja kanala koronarno. Apikalno instrumenti imaju dovoljno širok promjer da osiguraju adekvatnu dezinfekciju (82). TRN karakterizira povećana fleksibilnost. Fleksibilniji je do 3x više u odnosu na ProTaper Next (83).

## 1. 4. Recipročne tehnike instrumentacije korijenskih kanala

### 1.4.1. Recipročni pokret

Pokret instrumenta u smjeru suprotnom od smjera kretanja kazaljke na satu (engl. *counterclockwise, CCW*), pri kojem se reže dentin, naziva se recipročni pokret. Instrument se oslobađa pokretom u smjeru kazaljke na satu (engl. *clockwise, CW*). Izvlačenjem iz kanala uklanja se odrezani dentin koji je potrebno obrisati s instrumenta. Put koji instrument prijeđe u CCW smjeru veći je od onog u CW smjeru, što znači da je za potpunu rotaciju od 360° potrebno nekoliko recipročnih kretnji. Recipročna kretnja u odnosu na rotacijsku kretnju pokazuje sljedeće prednosti: potreban je manji broj instrumenata za čišćenje i oblikovanje korijenskog kanala, instrumenti rjeđe „zapinju" unutar kanala, čime je smanjena torzijska napetost; potreban je manji broj ciklusa unutar korijenskog kanala tijekom instrumentacije, što rezultira manjim opterećenjem instrumenta i smanjena je mogućnost loma instrumenta (84, 85). Osim toga dokazano je da je potrebno vrijeme instrumentacije kraće nego kod upotrebe istog instrumenta u punoj rotaciji (86). Gavini i sur. ( 2012) promatrali su fleksijski zamor instrumenata Reciproc 25 u pokretu kontinuirane rotacije i u recipročnom pokretu. Njihovi su rezultati pokazali da recipročni pokret povećava otpornost na fleksijski zamor u usporedbi s rotacijskim pokretom (87).

Postoji nekoliko varijacija recipročne kretnje uključujući:

- potpunu recipročnu kretnju (oscilirajuća kretnja)
- djelomičnu recipročnu kretnju (učinak rotacije)
- hibridnu recipročnu kretnju (kombinirana kretnja)

Hibridna recipročna kretnja može biti fiksna ili fleksibilna, tj. može se mijenjati vrsta recipročne kretnje u kanalu iz jedne u drugu, ovisno o mehaničkom otporu i okretnom momentu instrumenta u kanalu (88).

### 1.4.2. Povijesni razvoj recipročnih tehnika

Recipročna kretnja prvi je put predstavljena 1964. pojavom sustava Giromatic (MicroMega, Besancon, Francuska). Zatim su uslijedili kolječnici Intro-Endo 3LD (KaVo, Biberach, Njemačka) i Dynatrak sistem (Dentsply DeTrey, Konstanz, Njemačka). Ovi su motori omogućavali između 3000 i 6000 reciprokacija po minuti. Istovremeno je predstavljena zvučna verzija kolječnika sa sličnim instrumentima - Micro Mega 1500 Sonic Air Endo System (89).

Godine 1985. Roane & Sabala (90) opisuju posebno dizajniran čelični K-tip instrumenta (Flex-R-File). K označava tehniku uvijanja kojom je instrument proizveden. Instrument je imao modificirani vrh i koristio se u tzv. *stepdown* pokretu. U fazi umetanja instrumenta u korijenski kanal korištena je rotacija u smjeru kazaljke na satu do maksimalno 180°, a zatim rotacija u obrnutom smjeru od maksimalno 120°, uz tlačenje instrumenta u apikalnom smjeru (faza rezanja). Za izvlačenje instrumenta koristila se ponovno rotacija u smjeru kazaljke na satu. Ovu tehniku karakterizira poprilično široka instrumentacija u apeksnom dijelu (minimalno od veličine #45 u zavijenim, odnosno #80 u ravnim kanalima). Uporabom te tehnike bilo je značajno manje proguravanja detritusa kroz apeks (91). Uz navedene prednosti opisani su i nedostaci ove tehnike kao što su mogućnost perforacije korijena i loma instrumenata (92, 93). Pojavom Balanced force tehnike 1985. godine potisnute su navedene recipročne tehnike. Balanced force tehnika manualna je recipročna tehnika koja koristi instrumente od nehrđajućeg čelika većeg promjera u recipročnom pokretu. Tehnika zahtijeva vrijeme i često dovodi do proceduralnih pogrešaka (89).

Razvojem legure Ni-Ti proizvedeni su instrumenti koniciteta većeg od 0,04 (0,06 pa sve do 0,12). Njihova upotreba smanjuje neželjene komplikacije u obradi korijenskih kanala. Veći konicitet omogućuje da tijekom rotacije u kanalu instrument samo malom površinom dodiruje stijenku, čime se znatno smanjuje trenje (94, 95). Vrlo važna godina u razvoju Ni-Ti instrumenata bila je 2007. kada se pojavila tzv. *M-wire* tehnologija. *M-wire* Ni-Ti tehnologija temelji se na posebnoj termičkoj obradi legure koja stvara jači i fleksibilniji materijal, znatno pojačava otpornost na ciklička naprezanja i smanjuje mogućnost loma instrumenta (96, 97).

Nastojeći pojednostaviti instrumentaciju korijenskih kanala, kanadsko-libanonski znanstvenik Ghassan Yared razvio je koncept jednog instrumenta (30, 31). Primarna tehnika uključivala je uporabu samo jednog (0,08) ručnog, čeličnog instrumenta i apeks lokatora nakon što su određene prohodnost, radna dužina (WL) i upotreba samo jednog F2 ProTaper Ni-Ti

instrumenta (TulsaDentsply, Tulsa, OK, SAD). Instrument je korišten u kolječniku s motorom ATR Vision (ATR, Pistoia, Italija) s mogućnošću recipročnog pokreta (redukcija 16 : 1) u smjeru kazaljke na satu (CW) i u smjeru suprotnom od smjera kazaljke na satu (CCW). Instrument je pomican u kanalu tzv. pakirajućim pokretima (engl. *packing motion*) uz izuzetno male sile tlačenja prema apeksu, često čišćenje i ispiranje otopinom natrijeva hipoklorita. Budući da F2 ProTaper instrument nije primarno razvijen za recipročnu kretnju, u trenutku CW kretnje je zarezao dentin, a CCW kretnja oslobađala je instrument (CW kretnja bila je duža od CCW kretnje) pa se tako oblikovao konicitet kanala. Osim toga kombinacija CW i CCW kretnje, teoretski, smanjuje incidenciju torzijskog loma instrumenta. Yared (30) navodi da je u to doba prednost nove tehnike bila to što nije zahtijevala predtretman kanala ručnim instrumentima do broja #15 ili #20 čak i kod jako zavijenih kanala. Prva iskustva s novim pristupom instrumentaciji bila su pozitivna (98).

S obzirom na to da je F2 ProTaper Ni-Ti instrument korišten u recipročnoj kretnji zapravo konstruiran za konvencionalnu, rotacijsku tehniku, bilo je potrebno razviti nove, namjenske instrumente. Iz tog je razloga 2008. godine osam internacionalnih kliničara (Ben Johnson (SAD), Sergio Kuttler (SAD), Pierre Machtou (Francuska), Wilhem Pertot, (Francuska), Julian Webber (UK), JohnWest (SAD), Ghassan Yared (Libanon) i Clifford Ruddle (SAD)) u suradnji s Dentsply International započelo razvoj novog recipročnog instrumenta i pogonskog stroja. Četiri godine kasnije dvije su tehnike lansirane na tržište: Wave One (Dentsply) i Reciproc (VDW). U godinama koje su slijedile posebnom tehnikom toplinske obrade, koja utječe na molekularnu strukturu Ni-Ti legure, proizvedene su nove generacije instrumenata: Wave One Gold (Dentsply Sirona, Salzburg, Austrija) i Reciproc Blue (VDW, München, Njemačka).

Wave One Gold (Denstply) i Reciproc Blue (VDW) instrumenti izrađeni su od specijalno termički obrađene Ni-Ti legure koja ne posjeduje “memoriju oblika”, ali pokazuje povećanu fleksibilnost i otpornost na cikličko opterećenje (99, 100).

Da bi se istaknule prednosti i smanjili nedostaci recipročnih tehnika, nastala je adaptivna tehnika instrumentacije – Twisted File Adaptive (TFA) (Kerr, Orange, Kalifornija, SAD), čiji se instrumenti automatski prilagođavaju stresu u kanalu tijekom obrade. Kada se TFA instrument ne napreže unutar korijenskog kanala, njegova je kretnja kontinuirana rotacija, što omogućava bolju reznu učinkovitost i uklanjanje debrisa. Riječ je o isprekidanoj kretnji s CW-CCW kutovima od 600° do 0°, koja je jednako učinkovita kao kontinuirana rotacija u bočnom rezanju. Manja je incidencija jatrogenih pogrešaka, čime se smanjuje učinak „šarafljenja”

kojem su skloni Ni-Ti instrumenti velikog koniciteta. Pri povećanom naprezanju tijekom instrumentacije i zamoru metala kretnja TFA instrumenta mijenja se u recipročnu sa specifičnim kutovima koji variraju od 600° do 0° te od 370° do 50°, a mijenjaju se ovisno o anatomskim varijacijama i naprezanju unutar korijenskog kanala. Takva prilagodljiva kretnja smanjuje rizik od loma instrumenta bez utjecaja na učinkovitost jer Adaptive endomotor automatski bira najbolji pokret za svaku kliničku situaciju (101).

### 1.4.3. Reciproc tehnika instrumentacije

Godine 2011. predstavljena je Reciproc tehnika (VDW, Minhen, Njemačka) koja se sastoji od tri instrumenta R25 (crveni, 25/0,08), R40 (crni, 40/0,06), R50 (žuti, 50/0,05) i pripadajućeg motora. Instrumenti imaju poprečan presjek S-oblika i progresivan konicitet (49). Reciproc R25 instrument promjera je 0,25 mm na vrhu i 8 % koniciteta na prva 3 mm od vrha. Promjer na 16 mm (D16) je 1,05 mm. R40 promjera je 0,40 mm na D1, 6 % koniciteta prva 3 mm od vrha i D16 promjera od 1,10 mm. Treći instrument R50 ima D1 0,50 mm, 5 % konicitet i promjer na D16 od 1,17 mm (49). Instrumenti su proizvedeni od M-žice, posebnom termičkom obradom koja povećava fleksibilnost instrumenta i smanjuje ciklički zamor (102).

Kutovi su rotacije nejednaki i niži od kuta pod kojim se razvija elastični limit instrumenta. Posljedica je smanjeni torzijski zamor instrumenta, što tehniku čini manje osjetljivom i pouzdanijom. Dodatna prednost Reciproca njegova je efikasnost u revizijama kanalnog punjenja. Yared navodi da se Reciproc može koristiti u kanalu i bez postizanja prohodnosti kanala ručnim instrumentom (engl. *glide path*) (103).

Yoo i Choo uspoređivali su učinkovitost recipročnih tehnika Wave One i Reciproc s Pro Taper Universal i Profile rotacijskim tehnikama u obradi korijenskih kanala. Instrumenti recipročnih sustava koristili su se u pokretu lateralnog četkanja. Njihovi rezultati ukazuju na to da Reciproc i Wave instrumenti bolje prate anatomiju zavijenih korijenskih kanala nego ProTaper Universal i ProFile koji su pokazali tendenciju transportacije vanjskog zida kanala u apikalnoj trećini. Iz tog su razloga zaključili da ispitivani recipročni sustavi imaju dobru sposobnost oblikovanja kanala i da su pogodni za obradu kanala s jednim instrumentom (104).

Budući da su instrumenti predviđeni za jednokratnu uporabu, eliminirana je mogućnost unakrsne kontaminacije koja se povezuje s nemogućnošću adekvatnog čišćenja i sterilizacije prethodno korištenih instrumenata (102).

### 1.4.4. Recipročni instrumenti s površinski obrađenom legurom Ni-Ti

Da bi se poboljšala tehnika obrade korijenskih kanala i smanjila incidencija loma instrumenta, radilo se na unapređenju dizajna, poprečnog presjeka i načina uporabe instrumenta (105). Predstavljeni su novi procesi površinske obrade instrumenta, primjerice termička obrada legure, radi poboljšanja mehaničkih svojstava (45). Prva takva legura bila je M-žica, nakon nje predstavljena je i CM-žica (106). Instrumenti od CM-žice mogu se saviti prije uvođenja u kanal, imaju manju sklonost izravnavanju tijekom obrade korijenskog kanala i smanjenu učestalost grešaka tijekom instrumentacije. Ovi instrumenti pokazuju visok otpor na ciklički zamor (36, 107).

Termička obrada Ni-Ti instrumenata u novije je vrijeme u središtu pozornosti proizvođača jer je uočeno da se tako znatno može poboljšati fleksibilnost instrumenta i otpornost na ciklički zamor (108). Posebni procesi zagrijavanja i hlađenja rezultiraju vidljivim slojem oksida titana na površini instrumenta (99). Termomehanička obrada Ni-Ti legure dovodi do promjene u kristalnoj strukturi i pojave martenzične ili R-faze u kliničkim uvjetima. Dok su M-žica i instrumenti u R-fazi uglavnom u fazi austenita, CM-žica, Gold i Blue termički obrađeni instrumenti pretežno se sastoje od faze martenzita. Predstavnici recipročnih instrumenata s ovakvom obradom legure su Wave One Gold i Reciproc Blue. Budući da je martenzična faza dominantna, fleksibilniji su i otporniji na ciklički zamor i pokazuju veći kut (109). Osnovna je razlika između CM-žice i Gold, odnosno Blue, termički obrađenih instrumenata u tome što su recipročni instrumenti oblikovani prije termičke obrade (111).

Martenzični su instrumenti pogodni u obradi zavijenih korijenskih kanala. Korisno je što se mogu savijati prije uvođenja u kanal jer to olakšava premoštavanje stepenice nastale prethodnom obradom korijenskih kanala (36).

*1.4.4.1. Reciproc Blue (VDW, Minhen, Njemačka)*

Reciproc Blue (RCB) (VDW; WaveOne Gold, Dentsply Sirona Endodontics) napredna je verzija Reciproca, koja podliježe gore opisanom procesu termičke obrade nakon oblikovanja. Sustav se i dalje sastoji se od tri instrumenta: R25 (crveni, 25/0,08), R40 (crni 40/0,06), R50 (žuti, 50/0,05) i pripadajućeg motora za recipročnu kretnju.

Instrumenti su karakteristične plave boje. Fleksibilnost im je povećana za 40 %, a otpornost na ciklički zamor veća je dva do tri puta u odnosu na klasične Reciproc instrumente (111). Bolja učinkovitost postignuta je S-oblikom poprečnog presjeka, čime je omogućeno bolje ispiranje čak i jače zavijenih kanala (112). Konicitet, rezni kutovi i toplinski obrađena legura osiguravaju veću reznu učinkovitost. I ova tehnika instrumentacije koristi samo jedan instrument za obradu korijenskog kanala. Instrumenti nemaju memoriju oblika pa se prije instrumentacije mogu svinuti maksimalno 10° radi lakšeg pristupa kanalu. Sustav je moguće koristiti i za reviziju punjenja korijenskih kanala (113, 110).

## 1.5. Iatrogene pogreške tijekom instrumentacije korijenskog kanala

Iatrogene pogreške tijekom instrumentacije korijenskih kanala najčešće nastaju radi propusta kliničara (pogrešne manipulacije i nepažnje za detalje) ili potpuno nepredvidivo. Tu se ubrajaju: nastanak stepenice, blokada korijenskog kanala, perforacija korijena zuba, lom instrumenta i apikalna transportacija. Ove komplikacije otežavaju i/ili onemogućuju optimalan završetak preparacije korijenskog kanala i postizanje idealne radne duljine. Posljedica je nedovoljna dezinfekcija i manjkava obturacija korijenskih kanala. Prognoza takvog endodontskog liječenja također je nepovoljna (114).

### 1.5.1. Transportacija korijenskog kanala

Transportacija korijenskog kanala jest uklanjanje intrakanalnog dentina na konveksnom zidu korijenskog kanala. Do toga dolazi jer instrument nastoji vratiti se u svoj izvorni linearni oblik tijekom instrumentacije kanala. To se najčešće događa u apikalnom dijelu korijenskog kanala. Kao rezultat asimetričnog uklanjanja dentina tijekom preparacije uzdužna os kanala se pomjera, a kut zakrivljenosti se smanjuje, što rezultira ispravljanjem korijenskog kanala. Transportacija može uzrokovati gubitak apikalnog stopa i iritaciju perapikalnih tkiva ekstrudiranim debrisom, irigansima ili materijalima za punjenje (115).

Transportacija kanala povezana je s apikalnim curenjem (engl. *apical leakage*) (116, 117). Apikalna transportacija povezuje se s velikom količinom debrisa i mikroorganizama u apikalnom dijelu kanala, posebno ako se dogodi u ranijim stadijima preparacije.

Posljedice transportacije kanala su:

1. neadekvatna preparacija korijenskog kanala s velikom količinom debrisa i mikroorganizama u apikalnom dijelu kanala
2. prekomjerno uklanjanje dentina, što oslabljuje strukturu zuba i čini ga podložnijim frakturi
3. narušavanje integriteta korijena u slučaju apikalne ili strip perforacije (117).

### 1.5.2. Stepenica u korijenskom kanalu

Devijacija izvornog oblika korijenskog kanala bez komunikacije s parodontnim ligamentom označava se kao stepenica (engl. *ledge formation* ili *ledging*). Oblikovanje i čišćenje korijenskog kanala apikalno od stepenice otežano je, što često rezultira perzistentnim periapikalnim lezijama nakon intrakanalnog liječenja. Postoji uzročno-posljedična veza između formiranja stepenice i nepovoljnog ishoda endodontske terapije (118).

Uzroci formiranja stepenice su:

1. nedovoljno proširivanje pristupnog kaviteta
2. nedovoljna kontrola nad endodontskim instrumentom
3. pogrešna procjena smjera korijenskog kanala
4. pogrešno određena radna duljina
5. forsirano guranje instrumenta u kanalu
6. uporaba nesavijenog instrumenta od nehrđajućeg čelika koji je prevelik za zavijeni korijenski kanal
7. nepoštivanje sekvence instrumentacije
8. puna rotacija instrumenata koji za tu kretnju nisu predviđeni (proširivači i strugači)
9. neadekvatna irigacija i lubrikacija kanala tijekom instrumentacije
10. pokušaj uklanjanja slomljenog instrumenta
11. uklanjanje korijenskog punila tijekom revizije
12. pokušaj instrumentacije kalcificiranih korijenskih kanala
13. nehotično nabijanje debrisa u apikalni dio kanala, posljedica je apikalna blokada (118).

Najznačajnija morfološka karakteristika, koja utječe na nastanak stepenice je zavijenost korijenskih kanala. Posljedica nastanka stepenice je izravnavanje kanala (119- 122).

### 1.6. Sposobnost instrumenta da ostane centriran u kanalu tijekom instrumentacije

Sposobnost instrumenta da ostane centriran u kanalu tijekom obrade (sposobnost centričnosti engl. *centering ability*) odnosi se na praćenje izvorne anatomije kanala. Parametri koji na to utječu jesu: vrsta legure koja se koristi u proizvodnji instrumenta i dizajn instrumenta (poprečni presjek, konicitet, izgled vrška instrumenta) (123).

### 1.7. Mjerenje stupnja zavijenosti korijenskog kanala zuba

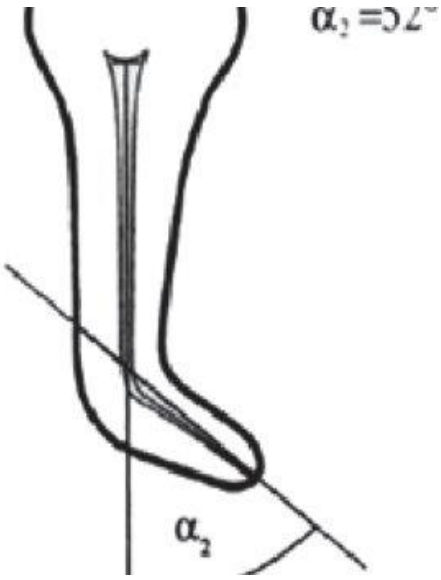
Oko 84 % ljudskih zuba pokazuje zavijenost korijenskih kanala različitog stupnja (124, 125). Jako zakrivljeni korijenski kanali rizični su čimbenik za nastanak proceduralnih pogrešaka tijekom instrumentacije, što može kompromitirati prognozu endodontskog liječenja (61, 126, 127, 128).

Budući da ne postoji konsenzus o idealnoj metodi za mjerenje zavijenosti korijenskih kanala, neke metode pogodnije su za kliničke, druge za istraživačke svrhe. Ovisno o parametrima na kojima se metoda temelji mogu se podijeliti u nekoliko skupina.

#### 1.7.1. Mjerenje kuta za određivanje zavijenosti korijenskih kanala

Prvi pokušaj mjerenja zavijenosti korijenskih kanala napravili su Fromme i sur. (129) tako što su na rendgenskoj snimci zuba spojili dvije tangente. Ova metoda bila je vrlo neprecizna s obzirom na to da je njome definirana samo promjena smjera uzdužne osi kanala.

Godinu dana kasnije, 1971. godine, Schneider et al. (130) definirali su tri kategorije zavijenosti korijenskih kanala: ravni (< 5°), umjereno zavijeni (od 10° do 20°) i jako zavijeni korijenski kanali (od 25° do 70°). Prva linija povučena je na rendgenskoj snimci zuba paralelno s dužinskom osi kanala. Druga linija polazi od apikalnog foramena, ide kroz kanal i siječe prvu liniju na mjestu gdje kanal napušta uzdužnu os zuba. Kut gdje se ove dvije linije sijeku predstavlja promjenu smjera uzdužne osi kanala u odnosu na uzdužnu os zuba (Slika 1).



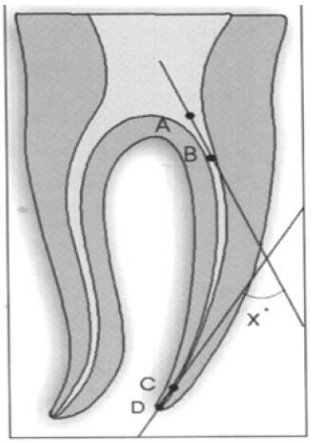

**Slika 1.** Metoda određivanja zavijenosti po Schneideru. Preuzeto iz Sonntag et al. (131)

Ova se metoda brzo proširila i često je citirana u literaturi.

Luiten i sur. (132) koristili su dvije linije definirane četirima geometrijskim točkama. Prva je točka u sredini ulaza u korijenski kanal (točka A), druga je točka 2 mm ispod ulaza, na uzdužnoj osi kanala (točka B). U apikalnoj trećini definirane su još dvije točke. Točka D nalazi se na sredini apikalnog foramena, točka C 1 mm iznad, na uzdužnoj osi kanala. Prva linija povučena je kroz točke A i B, druga kroz točke C i D. Kut koji ove dvije linije zatvaraju mjeren je kao zakrivljenost korijenskih kanala.

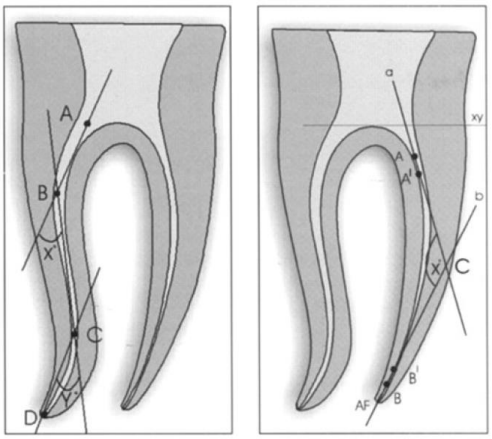
Ove tehnike nastoje unaprijediti Schneiderovu tehniku, daju jasniji prikaz morfologije koronarnog ulaza u kanal i apikalnog dijela kanala, a promjena smjera uzdužnog kanala od ulaza u kanal do apeksa jasnije je prikazana (Slika 2).

Ove metode omogućavaju uvid u višestruke promjene smjera uzdužne osi korijenskog kanala, ali ne govore o karakteristikama zavijenosti.




**Slika 2.** Metoda određivanja zavijenosti po Luitenu i suradnicima.
Preuzeto iz Sonntag et al. (131)

Cunningham i Senia (133) razvili su metodu za mjerenje multiplih krivulja korijenskih kanala (kanalna konfiguracija S-oblika). U tu svrhu određivali su kut zakrivljenosti u koronarnom i apikalnom dijelu kanala. Točka A središte je ulaza u korijenski kanal. Točka B na mjestu je gdje kanal počinje zavijati. Prva linija povezuje točke A i B. Druga linija povučena je od točke B do točke gdje se kanal opet zavija od uzdužne osi kanala (točka C). Četvrta linija prolazi od točke C do apikalnog foramena (točka D). Prednost ove tehnike nad Schneiderovom metodom jest mogućnost predstavljanja multiplih krivulja kod S-oblika korijenskog kanala. Osim toga kanalna je zakrivljenost određena u odnosnu na stvarnu konfiguraciju kanala.
Nedostatak ovih metoda proizvoljno je određivanje referentnih točaka duž uzdužne osi korijenskog kanala i linija koje ih povezuju.
Berbert i Nishiyama (134), uz grafičko određivanje promjene smjera uzdužne osi kanala, u svoju su metodu integrirali i matematičku komponentu. Ovo je prva metoda koja je omogućila da se opiše u kojem je dijelu maksimalna zakrivljenost kanala (Slika 3).

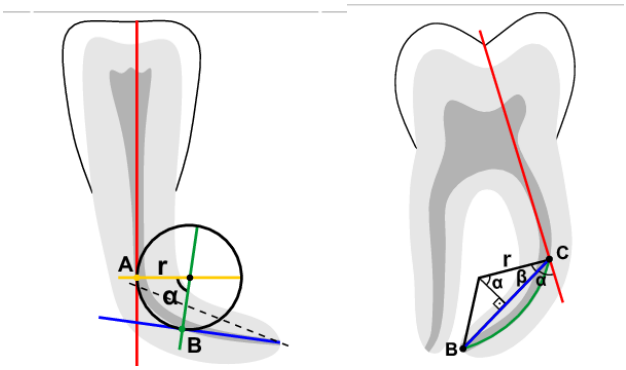



**Slika 3.** Metoda određivanja zavijenosti po Cunningham i Senia (lijevo) te po Berbert i Nishiyama (desno). Preuzeto iz Sonntag et al. (131)

### 1.7.2. Određivanje zavijenosti korijenskih kanala metodom kuta i kružnica

Pruet i sur. (135) razvili su metodu koja upotpunjuje mjerenje kuta po Schneideru s grafički određenim radijusom zakrivljenosti (Slika 4). Ovo je omogućilo prvo geometrijski točno opisivanje zavijenosti.

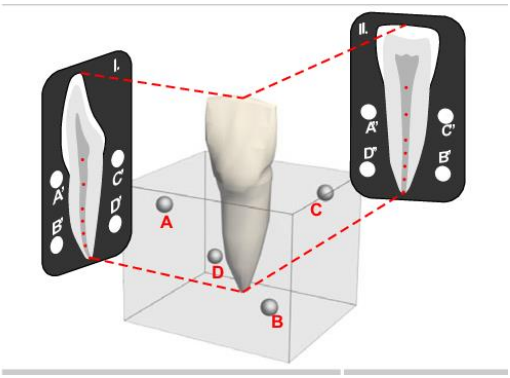
Modifikacija Pruetove metode jest tehnika po Schäferu, koja zavijenost kanala određuje pomoću kružnica koje definiraju zakrivljeni dio. Nedostatak metode jest njezina primjenjivost samo na određene konfiguracije kanala.




**Slika 4.** Metoda određivanja zavijenosti po Pruetu i sur. (lijevo) i po Schäferu i sur. (desno) Preuzeto iz Sonntag et al. (131)

### 1.7.3. Računalno potpomognuto određivanje zavijenosti korijenskih kanala

Prvi autori koji su matematički opisali zavijenost korijenskih kanala jesu Nagy i suradnici (136). Ova metoda primjenjiva je na sve kanalne konfiguracije. Prva točka mjerenja na apikalnom je foramenu, a ostalih šest točaka raspoređeno je do ulaza u korijenski kanal centralnom linijom uzdužne osi kanala. Pet od šest točaka u apikalnom su dijelu kanala, gdje se očekuje najveća zakrivljenost. Koordinate označenih točaka unose se u računalo i polinomskom funkcijom četvrtog stupnja izračunava se zavijenost korijenskih kanala.
Ova metoda nije naišla na odobravanje u praksi zbog kompleksne matematičke kalkulacije na kojoj se procedura temelji (Slika 5).

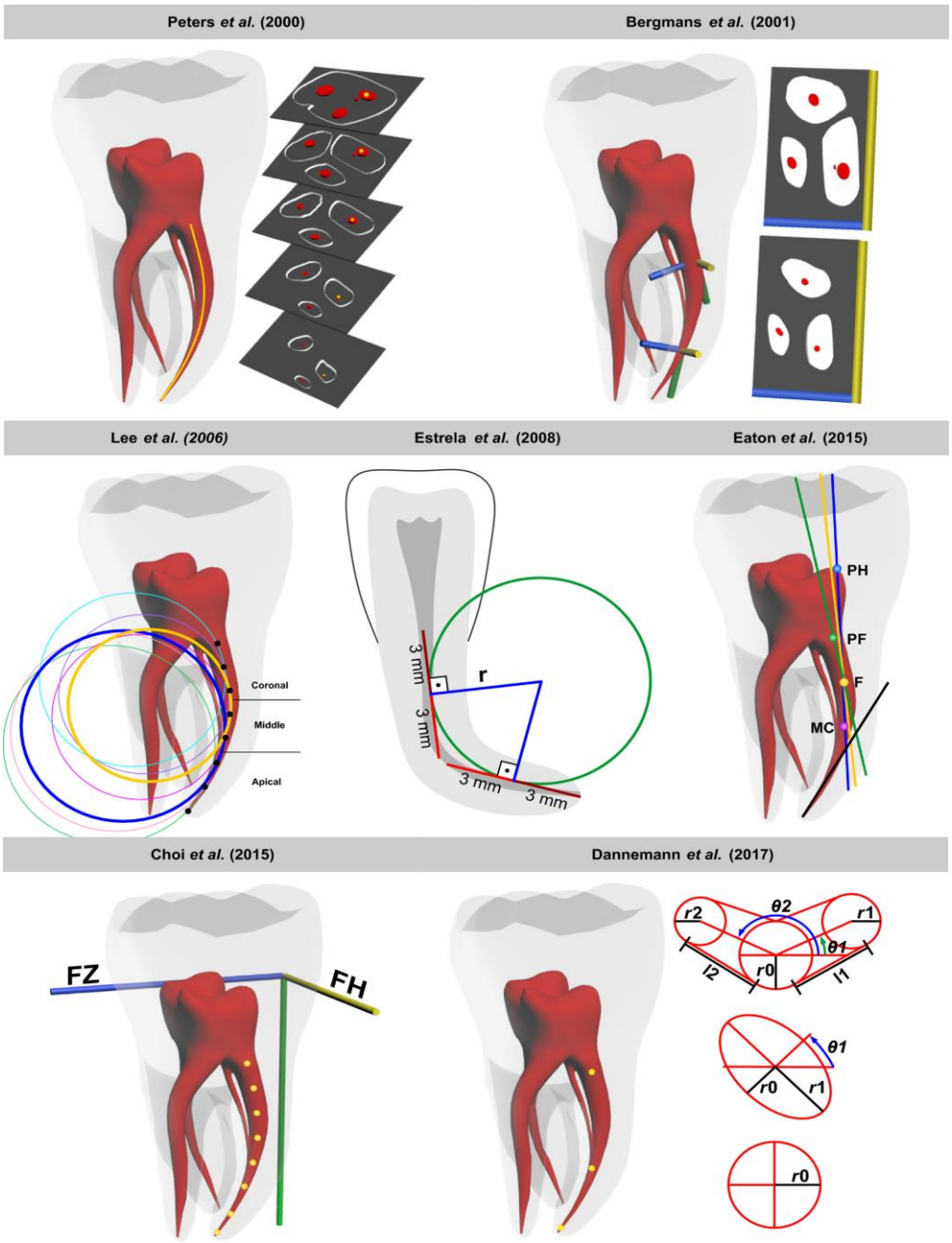



**Slika 5.** Metoda određivanja zavijenosti po Nagy i suradnicima
Preuzeto iz Sonntag et al. (131)

### 1.7.4. Trodimenzionalno određivanje zavijenosti korijenskih kanala

Sve spomenute metode temeljene su na dvodimenzionalnoj evaluaciji kanala. Međutim skoro svi kanali koji su zakrivljeni u meziodistalnoj ravnini pokazuju zakrivljenost i u bukooralnoj projekciji, što se ne može vidjeti na retroalveolarnoj rendgenskoj snimci zuba. Od pojave CBCT-a (engl. *Cone Beam Computed Tomography*) trodimenzionalni prikaz igra sve veću ulogu u analizi zavijenosti korijenskih kanala. U usporedbi s konvencionalnim CT-om, smanjeno je vrijeme i količina zračenja. Rezolucija CT-a neusporedivo je bolja, u svim ravninama, u odnosu na 2D rendgenske snimke. Istraživanja kanalne anatomije pomoću CBCT-a pokazala su korelaciju s histološkim istraživanjima kanalne morfologije (137 - 139). Park i sur. (140) i Dannemann i sur. (141) mjerili su zakrivljenost pomoću CBCT-a i računalnog softvera te prikazali kontinuirane krivulje duž korijenskog kanala. Ova metoda omogućila je

pouzdanu kvantifikaciju zavijenosti korijenskih kanala od apikalnog foramena do dna pulpne komore (Slika 6).




**Slika 6.** Trodimenzionalno određivanje zavijenosti korijenskih kanala po različitim autorima Preuzeto iz Sonntag et al. (131)

### 1.8. Mikro-kompjuterizirana tomografija u endodontskim istraživanjima

Mikro-kompjuterizirana tomografija (mikro-CT) neinvazivna je i precizna metoda koja se koristi u istraživanjima od 1980. godine. Ima bolju prostornu rezoluciju u odnosu na tradicionalni CT, proizvodi voksele u rasponu od 5 do 50 μm ili približno 1000000 puta manjeg volumena u usporedbi s CT vokselima (142, 143). Nedostatak mikro-CT analize jest što zahtijeva vrijeme, skupa je i klinički neprimjenjiva (*in vivo*).

U nedavnim istraživanjima u endodonciji mikro-CT primjenjuje se u analizi apikalne transportacije zavijenih korijenskih kanala i analizi površine intrakanalnog dentina nakon instrumentacije različitim tehnikama. Mikro-CT primjenjuje se i u analizi mineraliziranih tkiva kao što su zubi i kosti te materijala poput keramike i polimera (144, 145).

Istraživanja su pokazala učinkovitost i nedestruktivnost tehnike za mjerenje debljine cakline (146, 147). Točnost mjerenja pomoću mikro-CT-a uspoređena je s direktnim mjerenjima, mjerenjima 3D skenera i mjerenjima pomoću fotografija. Rezultati su pokazali da je mikro-CT izuzetno pouzdana i korisna metoda u mjerenju udaljenosti i analizi unutrašnjih i vanjskih struktura zuba (148).

Mikro-CT može točno i pouzdano prikazati presjeke zuba definiranjem debljine cakline, dentina i pulpne komore. Uz pomoć *imaging* softvera moguće je napraviti 3D rekonstrukcije koje daju prikaz volumetrijskih podataka za caklinu i dentin (tj. volumena cakline i dentina) (149).

U analizi morfologije zuba ovom neinvazivnom i preciznom metodom moguće je dobiti puno informacija: presjeci mogu biti rekonstruirani u bilo kojoj ravnini, a podaci se mogu prikazati kao dvodimenzionalne ili trodimenzionalne slike. Interna i eksterna anatomija mogu biti prikazane istovremeno ili odvojeno, a snimke se mogu analizirati kvalitativno i kvantitativno (150, 151).

U istraživanjima unutarnjih struktura zuba nekoliko je istraživača pomoću mikro-CT-a dobilo kvalitativne i kvantitativne rezultate mjerenja u analizi pulpne komore i morfologije korijenskih kanala. Razvijene su nove tehnike za izračunavanje volumena i zavijenosti korijenskih kanala pomoću micro-CT-a (152).

Bjorndal i sur. (153) pokazali su da je moguće napraviti 3D rekonstrukcije različitih dijelova zuba tako da se tvrda zubna tkiva prikažu transparentnim, a pulpna komora i sustav korijenskih kanala prikažu se opaknim. Pritom se rekonstruira i unutarnja i vanjska morfologija zuba kako

bi se sve cjelovito analiziralo. Dobiveni mikro-CT podaci služe kao baza u daljnjim analizama kanalne anatomije u eksperimentalnoj endodonciji, pretkliničkoj edukaciji o osnovnim endodontskim postupcima i kao vrijedan matematički model strukture zuba.

Jedna od najkompleksnijih varijacija kanalnog sistema je C-oblik kanala koji se najčešće pojavljuje kod drugih donjih molara. Rezultati istraživanja pomoću mikro-CT-a omogućili su dublje razumijevanje njihove anatomije i lakše predviđanje rezultata liječenja (154 - 156). Uz pomoć mikro-CT-a istraživanja i usporedba različitih endodontskih sistema za obradu korijenskih kanala postala je jednostavna (157). Dobivene informacije omogućuju mjerenja prije i poslije preparacije. Mjere se: površina i volumen korijenskog kanala, količina uklonjenog dentina, debljina kanala (poluprečnik), (ne)instrumentirana površina, zavijenost, transportacija kanala, izravnavanje kanala i centriranje instrumenta u kanalu. Osim toga analizira se revizija kanalnog punjenja (138, 144, 156 - 158).

# 2. CILJEVI I HIPOTEZE

Ciljevi doktorskog rada su:

1. Dizajnirati model određivanja zavijenosti korijenskih kanala mikro-kompjuteriziranom tomografijom (mikro-CT-om) i na temelju standardiziranog modela odabrati uzorke za istraživanje.
2. Odrediti i usporediti stupanj transportacije zavijenih korijenskih kanala nakon instrumentacije zavijenih kanala rotacijskim tehnikama (ProTaper Next, TruNatomy), recipročnim tehnikama (Reciproc, Reciproc Blue) i ekspandirajućom XP-Endo Shaper tehnikom instrumentacije kanala.
3. Odrediti i usporediti centričnost testiranih instrumenata u kanalu tijekom instrumentacije zavijenih korijenskih kanala.

Nulte hipoteze istraživanja su:

1. Nema razlike u stupnju transportacije zavijenih korijenskih kanala nakon instrumentacije rotacijskom (ProTaper Next, TruNatomy), recipročnim tehnikama (Reciproc, Reciproc Blue, Wave One Gold) i XP-EndoShaper tehnikom instrumentacije.
2. Nema razlike u centričnosti instrumenta u zavijenim korijenskim kanalima tijekom instrumentacije rotacijskom (ProTaper Next, TruNatomy), recipročnim tehnikama (Reciproc, Reciproc Blue, Wave One Gold) i XP-EndoShaper tehnikom instrumentacije.

Radne hipoteze znanstvenog istraživanja:

1. Postoji razlika u stupnju transportacije zavijenih korijenskih kanala nakon instrumentacije rotacijskom (ProTaper Next, TruNatomy), recipročnim tehnikama (Reciproc, Reciproc Blue, Wave One Gold) i XP-EndoShaper tehnikom instrumentacije.
2. Postoji razlika u centričnosti instrumenta u zavijenim korijenskim kanalima tijekom instrumentacije rotacijskom (ProTaper Next, TruNatomy), recipročnim tehnikama (Reciproc, Reciproc Blue, Wave One Gold) i XP-EndoShaper tehnikom instrumentacije.

# 3. MATERIJALI I POSTUPCI

### 3.1. Odabir uzoraka za istraživanje

Istraživanje je odobrio Etički odbor Stomatološkog fakulteta Sveučilišta u Zagrebu na XXIII. redovnoj sjednici (Broj: 05-PA-15-12/2017). Za određivanje veličine uzorka napravljena je *power* analiza, koristeći hi-kvadrat test i analizu varijance (G*Power 3.1 software; Heinrich Heine Univerzitet, Düsseldorf, Njemačka) s a = 0.05 i b = 0.95 kako bi se odredila veličina uzorka po grupi. *Power* analizom izračunato je da treba biti 10 zuba po grupi.

Za istraživanje je korišteno 50 humanih izvađenih gornjih prvih i drugih molara. Kriteriji uključivanja zuba bili su: potpuno razvijeni korijeni zuba bez znakova eksterne ili interne resorpcije, intrakanalnih kalcifikacija, karijesa korijena i bez prethodnog endodontskog liječenja. Za istraživanje su korišteni mezijalni kanali koji su po svojoj anatomiji okruglog oblika. Intrakanalna anatomija analizirana je na CBCT snimkama. Izvađeni zubi snimani su (Cranex 3DX, Soredex, Tuusula, Finska) uz upotrebu parametara CBCT-a:
vidno polje 5 × 5 (5.0 mm) mm; ENDO mode, 85 µm; 6.3 mA; 90 kV; 8.7 s; 450.3 mGycm$^2$. Prisutnost dvaju odvojenih mezijalnih kanala (anatomija po Vertucciju tip IV) potvrđena je postavljanjem dvaju proširivača veličine #10 (Dentsply-Sirona Endodontics, Ballaigues, Švicarska) u meziobukalni i meziolingvalni kanal sve dok vrhovi instrumenata nisu bili vidljivi na apikalnom otvoru obaju kanala. Ova konfiguracija kanala dodatno je potvrđena pomoću CBCT-a.

### 3.2. Priprema zuba za istraživanje

Zubi su, nakon vađenja, pohranjeni u 0,1 % otopinu timola do primjene. Zubi su trepanirani dijamantnim svrdlom broj 016 (Komet, Rock Hill, SC, SAD) uz vodeno hlađenje. Prohodnost mezijalnih korijenskih kanala potvrđena je proširivačem veličine #10 (Dentsply Maillefer, Ballaigues, Švicarska) prije i nakon instrumentacije. Radna duljina kanala određena je proširivačem veličine #10 ili #15 (Dentsply/Maillefer, Ballaigues, Švicarska) i definirana je na 1 mm od apeksa pomoću stereomikroskopa. Kvržice zuba skraćene su kako bi se radna duljina svih uzoraka standardizirala na okvirno 18 mm.

### 3.3. Mjerenje zavijenosti kanala mikro-kompjuteriziranom tomografijom

Upotreba mikro-kompjuterizirane tomografije omogućava više načina modeliranja zavijenosti korijenskih kanala. Budući da se radi o prostornoj metodi, u ovom je radu odabran pristup koji se temelji na selekciji svih točaka koje leže na jednom boku korijenskog kanala po čitavoj dužini kanala. Selekcija točaka provedena je poluautomatski i to tako da je ručno odabrano nekoliko točaka po dužini korijenskog kanala, nakon čega je tako definiranom putanjom provedena automatska selekcija svih točaka boka korijenskog kanala. Automatska selekcija provedena je korištenjem Polyline fit alata dostupnog u Volume Graphics VG Studio Max softverskom paketu (Slika 7). Nakon što je na prethodno opisani način dobiven set točaka koji odgovara odabranom boku korijenskog kanala (Slika 8), podaci su izvezeni u standardni tekstualni format (csv).

Model izračuna zavijenosti korijenskih kanala temelji se na sljedećim koracima:

1. Izračunate su jednadžbe pravaca između (n-1) i (n)-te točke, te između (n) i (n + 1)-te točke
2. Izračunat je kut između dobivenih pravaca (Slika 8)
3. Koraci 1) i 2) ponavljaju se za cijeli set podataka, odnosno za sve točke analiziranog korijenskog kanala
4. Svi izračunati kutevi zbrajaju se i potom dijele s ukupnim brojem točaka, čime se dobiva normalizirana srednja vrijednost kuta koja ne ovisi o broju točaka (budući da postoje razlike u duljini, odnosno broju točaka pojedinih korijenskih kanala).

Ovako postavljen matematički model omogućava jednostavnu i brzu relativnu usporedbu zavijenosti korijenskih kanala istih zuba prije i poslije instrumentacije. Iako opisani model nije pogodan za iskazivanje apsolutnih iznosa zavijenosti, njegova je prednost u povećanoj osjetljivosti na promjene u geometriji korijenskih kanala. Nadalje model je osjetljiv i na prostorno lokalizirane promjene, odnosno uzima u obzir i promjene u stanju površine koje mogu nastupiti prilikom instrumentacije. U smislu predmetnog istraživanja, opisani model primijenjen je na mikro-CT rezultate zuba prije i nakon instrumentacije, nakon čega je usporedbom normaliziranih srednjih vrijednosti kuta moguće statistički obraditi nastale promjene.

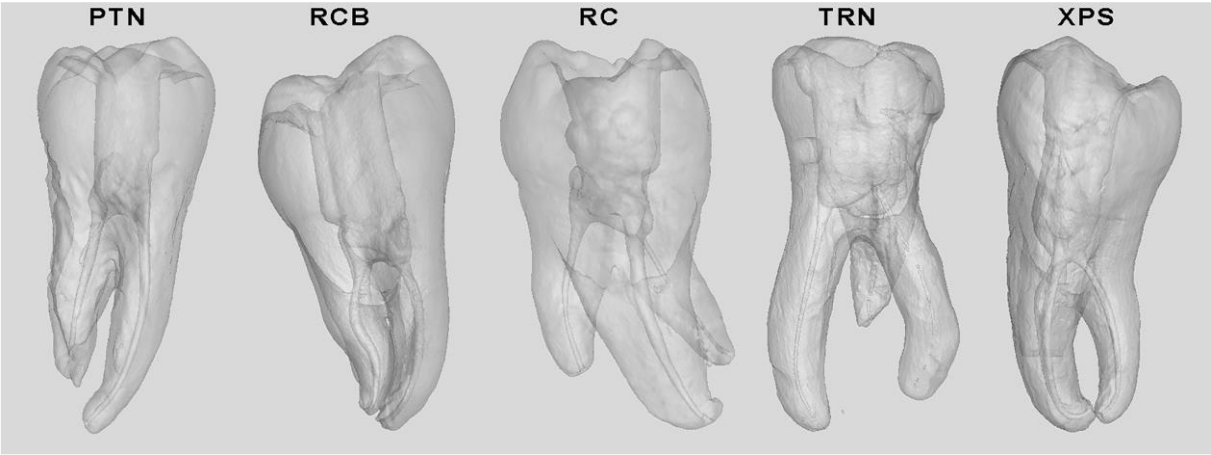
**Slika 7.** Primjer selekcije korijenskog kanala primjenom Polyline alata u VG studio Max softverskom paketu

**Slika 8.** 2D prikaz točaka korijenskog kanala iz slike 1 (gornja slika) i uvećani prikaz rada primijenjenog algoritma

### 3.4. Instrumentacija korijenskih kanala

Pripremljeni uzorci raspoređeni su metodom slučajnog odabira (http://www.random.org) u pet skupina ovisno o korištenoj tehnici instrumentacije.

U svakoj skupini bilo je 10 uzoraka (Slika 9). Svaki instrument korišten je za instrumentaciju triju kanala. Kanali su prije i tijekom instrumentacije ispirani s 4 ml 2,5 % natrijevog hipoklorita (NaOCl), a nakon svakog instrumenta provjerena je prohodnost apikalnog otvora ručnim instrumentom, proširivačem veličine #10.




**Slika 9.** Mikro-CT snimke reprezentativnih primjera molara korištenih u istraživanju za svaku skupinu instrumentacije (PTN-ProTaper Next; RCB-Reciproc Blue; RC-Reciproc; TRN-TruNatomy; XPS-XP-Endo Shaper)

*Skupina 1: Strojna rotacijska tehnika instrumentacije ProTaper Next (Dentsply Sirona, Ballaigues, Švicarska)*

Prema preporukama proizvođača za instrumentaciju korišten je endomotor s navedenim postavkama (Wave One Gold, Dentsply Sirona): brzina rotacije od 300 okretaja u minuti i okretni moment 2,5 N/cm$^2$. Nakon uvođenja u kanal instrument je napredovao prema apikalno pakirajućim pokretima unutra-van (engl. *in and out pecking motion*) uz amplitudu od 3 mm i lagani apikalni pritisak te četkastim pokretima prema lateralnim zidovima. Nakon triju pokreta unutra-van instrument je izvađen iz kanala i očišćen sterilnom gazom.

Korijenski kanali instrumentirani su ProTaper Next instrumentima X1 i X2 (Slika 10).

**Slika 10.** ProTaper Next instrumenti X1 i X2

*Skupina 2. Recipročna tehnika instrumentacije, Reciproc (VDW, Njemačka)*

U ovom istraživanju korišten je instrument Reciproc 25 (Slika 11) s endomotorom za recipročnu kretnju (VDW, Minhen, Njemačka) uz postavku Reciproc All.

Instrument je uveden u kanal uz lagani apikalni pritisak. Korišteni su pakirajući pokreti instrumenta do postizanja pune radne duljine.

**Slika 11.** Instrument Reciproc R25

*Skupina 3. Recipročna tehnika instrumentacije, Reciproc Blue (VDW, Njemačka)*

Za instrumentaciju je korišten instrument Reciproc Blue 25 (Slika 12) kako je opisano i za Skupinu 2.

**Slika 12.** Instrument Reciproc Blue

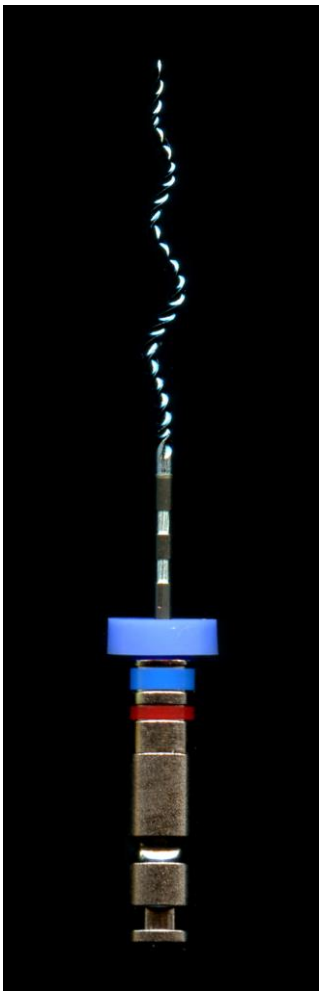
*Skupina 4: Rotacijska tehnika instrumentacije, TruNatomy (Dentsply Sirona)*

Instrumentacija kanala započinje s TruNatomy Orifice Modifier (20/08) uz tri lagana pokreta s amplitudom 2 - 5 mm. Zatim se u kanal ulazi s TRN Prime shaping instrumentom (25/04) (Slika 13) u motoru Wave One Gold (Dentsply Sirona) uz brzinu od 500 okretaja u minuti i okretni moment 1,5 N/cm$^2$. Instrument je korišten na gore opisani način.

**Slika 13.** TruNatomy Orifice Modifier i Prime shaping instrumenti

*Skupina 5: Ekspandirajući instrument XP-Endo Shaper (FKG)*

Zubi pete skupine instrumentirani su s XP-Endo Shaper instrumentom (30/ minimalni konicitet 04) (Slika 14). Instrument je korišten u VDW Gold motoru uz brzinu od 800 okretaja u minuti i okretni moment od 1 N/cm$^2$. Postupak rada isti je kao u prethodnim grupama. Dovoljno je vremena posvećeno kako bi instrument ekspanzijom i kontrakcijama postigao optimalan oblik korijenskog kanala.



Slika 14. Ekspandirajući instrument XP-Endo Shaper (FKG)

Instrumentacija se smatrala završenom kada je instrument dosegnuo radnu duljinu tri puta.
Za instrumentaciju kanala korišteno je ukupno 7 mL 2,5 % NaOCl, koja je u kanal dostavljena pomoću šprice od 2 mL i 31G igle (Steri Tips, DiaDent, Njemačka). Igla je postavljena 2 mm od apikalnog foramena.
Nakon instrumentacije uslijedilo je završno ispiranje korijenskih kanala radi uklanjanja zaostatnog sloja. Protokol završnog ispiranja sastojao se od kontinuiranog ispiranja s 2 mL 2,5 % NaOCl 30 sekundi, 15 % EDTA (Calsinase, Lege artis, Dettenhausen, Njemačka), 2 mL tijekom 2 min i 2 mL 2,5 % NaOCl 30 sekundi (po kanalu), praćeno s 2 mL fiziološke otopine. Preostali irigans aspiriran je iz kanala istom iglom. Kanali su posušeni suhim sterilnim papirnim poenima. Napravljene su nove mikro-CT snimke koje su rekonstruirane u skladu s inicijalno definiranim parametrima.

### 3.5. Mikro-CT snimanje uzoraka

Uzorci su skenirani mikro-CT uređajem (NIKON XT H 225; Nacionalni laboratorij za duljinu Fakulteta strojarstva i brodogradnje) prije i nakon instrumentacije korijenskih kanala. Protokol skeniranja definiran je nakon preliminarnih mjerenja. Parametri CT skenova bili su optimirani prema definiranim uzorcima radi postizanja što višeg odnosa signal - šum (SNR engl. *signal to noise ratio*). U konačnici su kao optimalni odabrani napon izvora x-zraka iznosa 110 kV, struja izvora x-zraka iznosa 240 µA i predfiltriranje x-zraka s bakrenim filtrom debljine 0,1 mm.

Svaki CT sken snimljen je s 1440 projekcija, odnosno s kutom zakreta između projekcija u iznosu od 0,25°, pri čemu je kod snimanja svake projekcije zaustavljena rotacija uzorka i snimljen prosjek dviju uzastopnih ekspozicija. Pojedinačno vrijeme ekspozicije iznosilo je 333 ms, odnosno 666 ms za svaku projekciju zbog dvostrukog eksponiranja.

Svaka grupa uzoraka skenirana je pojedinačnim CT skenom, a uzorci su smješteni u standardni držač načinjen od stiropora. Ova strategija osigurava izloženost svakog uzorka unutar grupe istim uvjetima mjerenja. Nadalje uzorci su uvijek pozicionirani na istom mjestu u volumenu mjerenja CT-a osiguravajući standardiziranu magnifikaciju između različitih grupa. Ovaj pristup rezultirao je u voksel veličini od 45 µm, koja je bila konstantna za sve analizirane vrste.

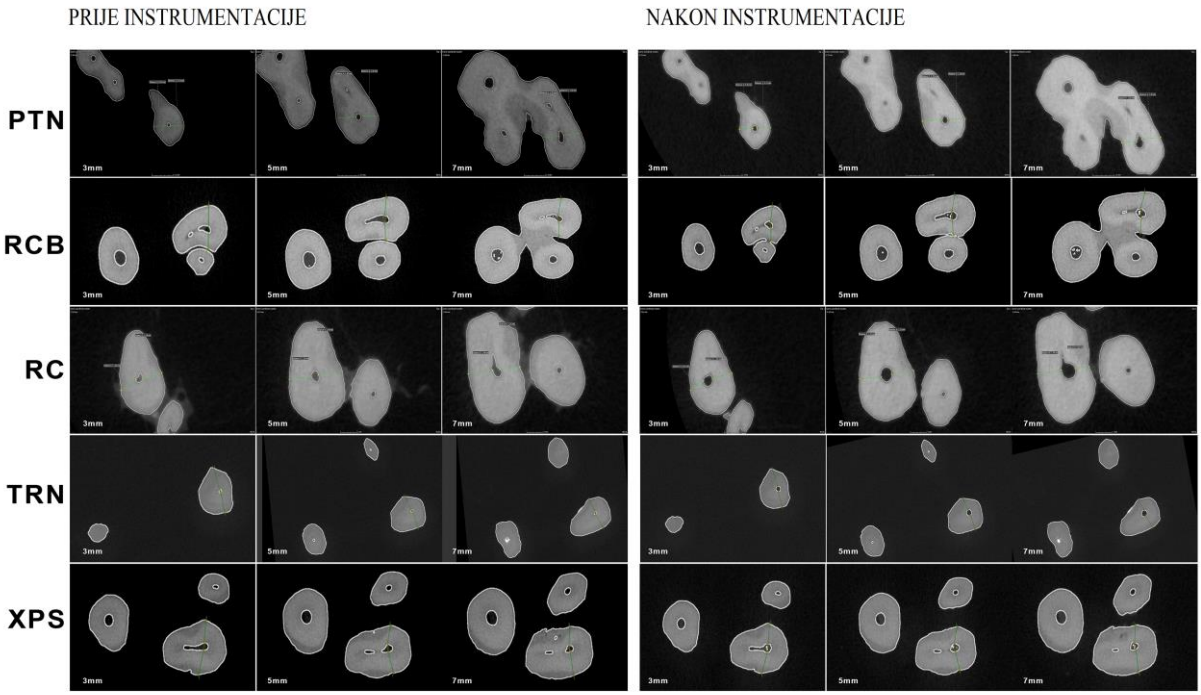
Nakon snimanja uzoraka načinjene su 3D rekonstrukcije pomoću Nikon CT Pro softvera.

Korekcija selektivnog prigušivanja x-zraka u materijalu (engl. *beam hardening*) provedena je primjenom polinoma 5. reda, a njihovi su koeficijenti odabrani metodom najmanjih kvadrata. Nakon te korekcije na cijeli je volumen primijenjen median filter s matricom 3x3. Time se dodatno povećava odnos signal - šum. Tako obrađene projekcije rekonstruirane su u 3D volumene koji su potom segmentirani u softverskom paketu Volume Graphics VG Studio Max 3.2. Svaki pojedinačni uzorak izdvojen je kao zasebna datoteka volumena i označen nazivom te rednim brojem grupe.

Nakon toga na volumene uzoraka primijenjen je adaptivni algoritam za definiranje granice površina-zrak (engl. *VG Studio Max Advanced surface determination*) s točnošću ispod razine voksela. Nakon što je time definirana površina pojedinog uzorka, provedeno je preklapanje uzoraka prije i poslije instrumentacije, pri čemu je korištena metoda najmanjih kvadrata kako bi se minimizirala odstupanja u preklapanju. Ovim je pristupom osigurano konzistentno dimenzionalno mjerenje, poput mjerenja transportacije, u uzorcima prije i poslije instrumentacije.

### 3.6. Mjerenje transportacije kanala nakon instrumentacije

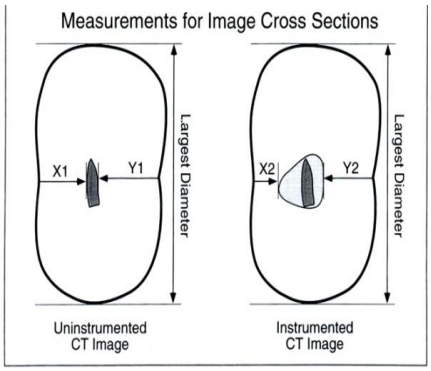
Svaki pojedinačni uzorak služio je kao kontrola samome sebi. Transportacija kanala izračunata je u meziodistalnom smjeru u milimetrima uz upotrebu formule po Gambillu i suradnicima (1996) ([X1_X2]_[Y1_Y2]) prije i nakon instrumentacije.
X1 je najkraća udaljenost između mezijalnog dijela korijena i stijenke neinstrumentiranog kanala, X2 je najkraća udaljenost između mezijalnog dijela korijena i stijenke instrumentiranog kanala, Y1 je najkraća udaljenost između distalnog dijela korijena i stijenke neinstrumentiranog kanala i Y2 je udaljenost između distalnog dijela korijena i stijenke instrumentiranog kanala.
Za evaluaciju su odabrani poprečni presjeci korijena na udaljenosti 3, 5 i 7 mm od anatomskog apeksa. Rezultat 0,0 označavao je izostanak kanalne transportacije, negativan rezultat kanalnu transportaciju od područja furkacije (u distalnom smjeru), a pozitivan rezultat transportaciju prema području furkacije (u mezijalnom smjeru) (Slika 15).




**Slika 15.** Mikro-CT snimke poprečnog presjeka korijenskih kanala prije i nakon instrumentacije različitim tehnikama. Poprečni presjeci napravljeni su na razini od 3 mm, 5 mm i 7 mm od apikalnog foramena

### 3.7. Analiza centričnosti instrumenta u korijenskom kanalu

Sposobnost instrumenta da ostane centriran unutar kanala (engl. *centering ability*) izračunata je na 3, 5 i 7 mm od anatomskog apeksa koristeći formulu (X1-X2) /(Y1-Y2) (159) (Slika 16).




**Slika 16.** Mjerenje centričnosti instrumenta tijekom instrumentacije
Preuzeto iz Gambill et al. (159)

Kada navedene vrijednosti nisu jednake, manja brojka smatra se brojnikom omjera.
Prema ovoj formuli rezultat 1 znači savršenu centriranost instrumenta unutar kanala, a vrijednosti bliže 0 ukazuju na smanjenu sposobnost instrumenta da ostane centriran unutar kanala (160).

### 3.8. Statistička analiza

Za analizu rezultata korišten je jednosmjerni ANOVA test s odgovarajućim post-hoc testom. Svi rezultati imali su parametarsku raspodjelu prema Kolmogor-Smirnovom testu. Razina značajnosti testa postavljena je na 0,05 i korištena je licencirana IBM SPSS Statistics verzija 25.

# 4. REZULTATI

Tijekom instrumentacije kanala, niti jedan instrument nije pukao.

Tablica 1. pokazuje vrijednosti transportacije zavijenih kanala za testirane tehnike instrumentacije: PTN, RCB, RC, TRN i XPS.

Tablica 2. pokazuje vrijednosti centričnosti instrumenata PTN, RCB, RC, TRN i XPS tijekom instrumentacije zavijenih korijenskih kanala.

**Tablica 1.** Ukupna kanalna transportacija po skupinama (u mm) i kanalna transportacija na udaljenosti 3, 5 i 7 mm od anatomskog apeksa nakon instrumentacije zakrivljenih korijenskih kanala s pet različitih tehnika instrumentacije

| **Eksperimentalne skupine** | **Transportacija kanala (udaljenost u mm od apeksa)** | | | | | |
|---|---|---|---|---|---|---|
| | **Ukupno** | **95% interval pouzdanosti za aritmetičku sredinu** | | **3 mm** | **5 mm** | **7 mm** |
| | | **Donja granica** | **Gornja granica** | | | |
| ProTaper Next (PTN) | 0,008 ± 0,011[a] | -0,015 | 0,030 | 0,014 ± 0,021[a] | -0,015 ± 0,014[a] | 0,025 ± 0,021[a] |
| Reciproc Blue (RCB) | 0,099 ± 0,035[b] | 0,027 | 0,171 | -0,021 ± 0,051[a] | 0,124 ± 0,052[b] | 0,195 ± 0,061[b] |
| Reciproc (RC) | 0,023 ± 0,037[ab] | -0,055 | 0,101 | 0,022 ± 0,047[a] | -0,038 ± 0,069[a] | 0,084 ± 0,076[b] |
| TruNatomy (TRN) | -0,020 ± 0,019[a] | -0,058 | 0,018 | 0,009 ± 0,024[a] | 0,014 ± 0,020[a] | -0,082 ± 0,040[a] |
| XP-endo Shaper (XPS) | -0,020 ± 0,020[a] | -0,061 | 0,020 | 0,021 ± 0,014[a] | -0,024 ± 0,033[a] | -0,058 ± 0,045[a] |

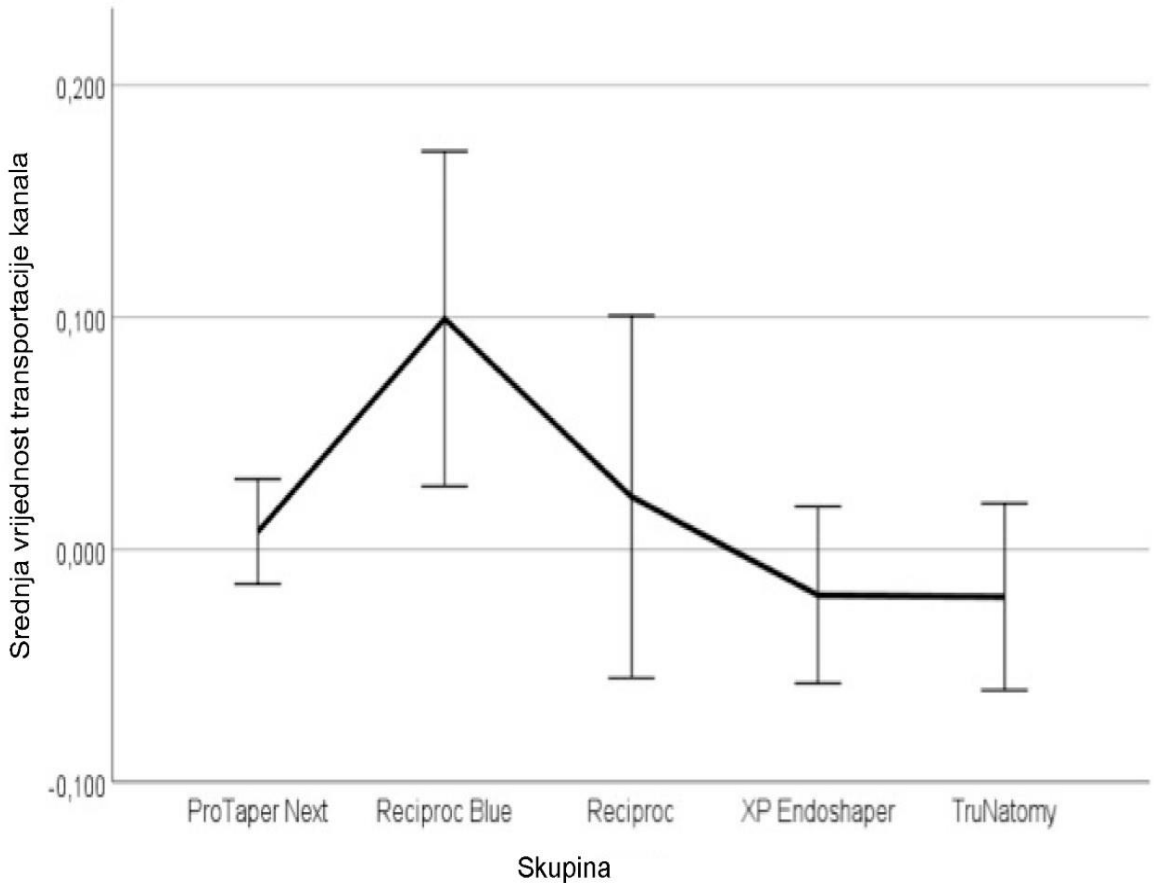
[a,b] Pojedina slova unutar stupca označavaju u odnosu na koju skupinu se odnosi značajna p vrijednost

**Tablica 2**. Ukupna centričnost testiranih instrumenata (u mm) i centričnost instrumenata na udaljenosti 3, 5 i 7 mm od anatomskog apeksa tijekom instrumentacije zavijenih korijenskih kanala

| Eksperimentalne skupine | Centričnost instrumenta unutar kanala (udaljenost u mm od apeksa) | | | | | |
|---|---|---|---|---|---|---|
| | Ukupno | 95% interval pouzdanosti za aritmetičku sredinu | | 3 mm | 5 mm | 7 mm |
| | | Donja granica | Gornja granica | | | |
| ProTaper Next (PTN) | 0,575 ± 0,045[a] | 0,482 | 0,667 | 0,592 ± 0,085[a] | 0,579 ± 0,075[a] | 0,553 ± 0,082[a] |
| Reciproc Blue (RCB) | 0,402 ± 0,049[b,c] | 0,301 | 0,502 | 0,357 ± 0,085[a] | 0,490 ± 0,103[a] | 0,358 ± 0,062[a] |
| Reciproc (RC) | 0,420 ± 0,065[b,c] | 0,284 | 0,557 | 0,470 ± 0,129[a] | 0,038 ± 0,103[a] | 0,314 ± 0,111[a] |
| TruNatomy (TRN) | 0,527 ± 0,051[a,c] | 0,422 | 0,632 | 0,514 ± 0,094[a] | 0,014 ± 0,102[a] | 0,453 ± 0,068[a] |
| XP-endo Shaper (XPS) | 0,486 ± 0,058[a,c] | 0,367 | 0,605 | 0,510 ± 0,098[a] | 0,024 ± 0,092[a] | 0,377 ± 0,109[a] |

[a,b,c] Pojedina slova unutar stupca označavaju u odnosu na koju skupinu se odnosi značajna p vrijednost

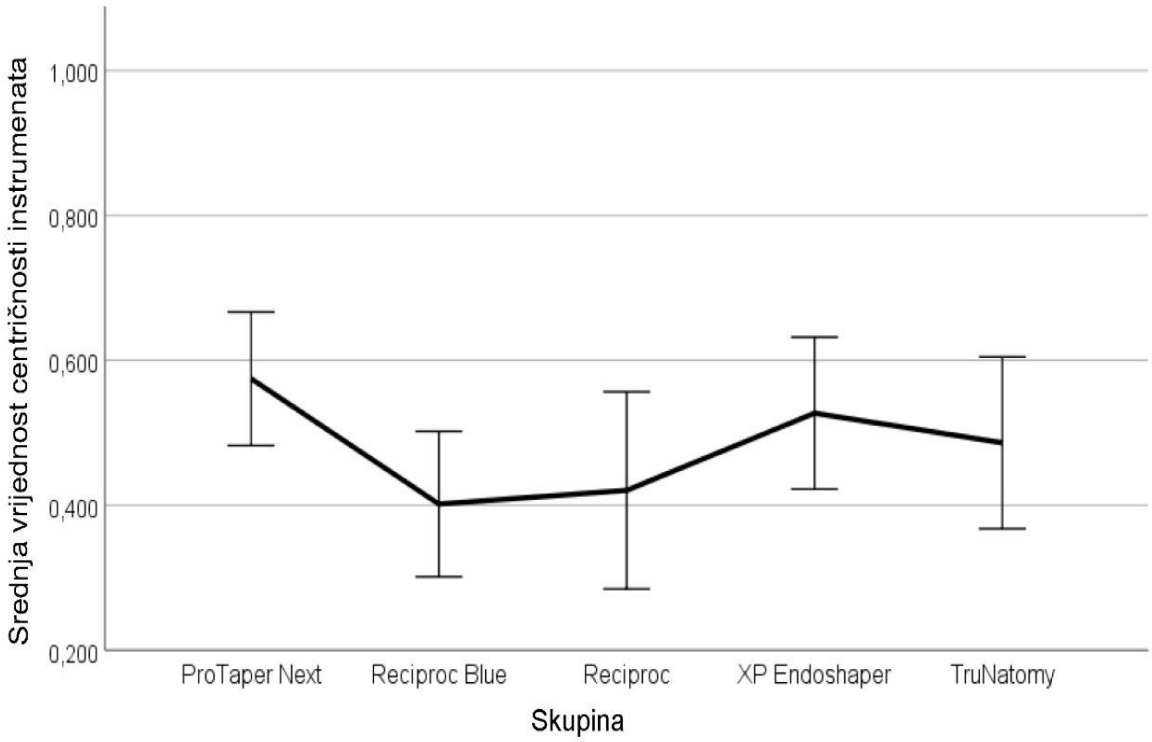
RCB je uzrokovao značajno veću transportaciju kanala u usporedbi s ostalim ispitivanim tehnikama ($p < 0,05$). Nije bilo statistički značajne razlike u transportaciji kanala između skupina PTN, RC, XPS i TRN ($p > 0,05$) (Slika 17.).




**Slika 17.** Ukupna srednja vrijednost transportacije zavijenih korijenskih kanala nakon instrumentacije s pet različitih tehnika

Analiza centričnosti instrumenta tijekom obrade kanala pokazuje da PTN ima značajno bolju sposobnost da ostane centriran u korijenskom kanalu (najveća prosječna vrijednost, koja je najbliža 1) u usporedbi s RC i RCB tehnikama (p = 0,046, p = 0,017).

Između ostalih testiranih tehnika nije bilo razlika u centričnosti (p > 0,05) (Slika 18).

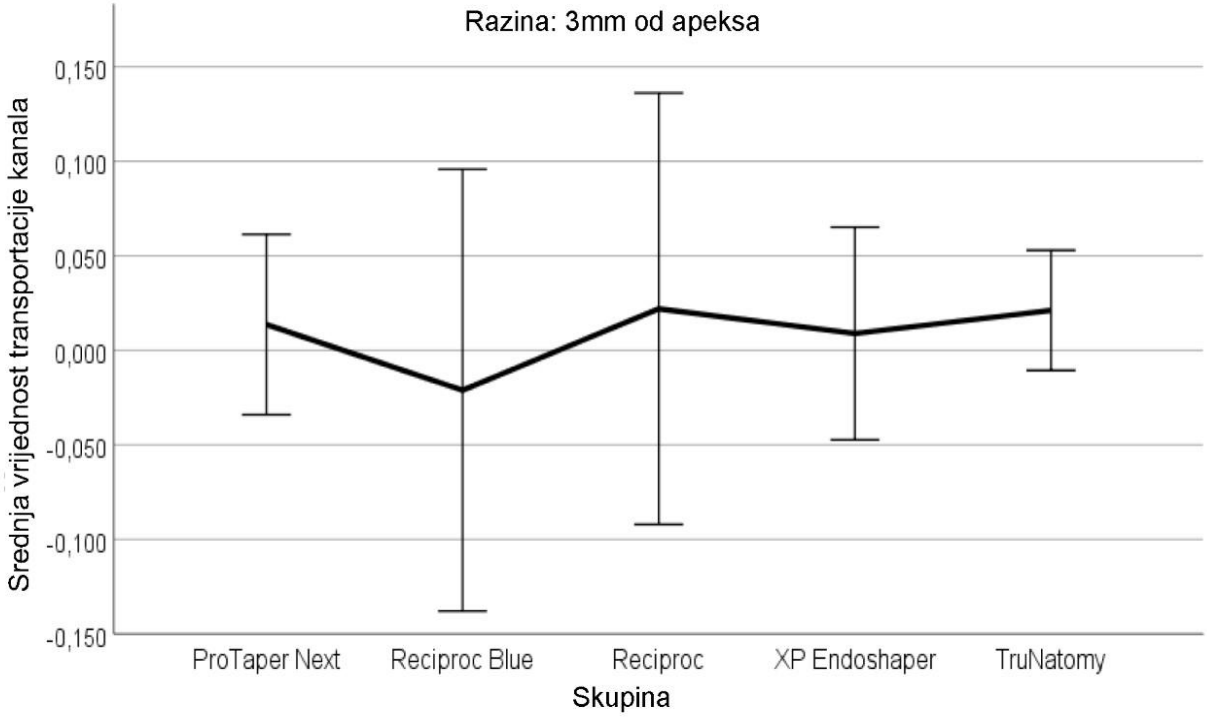



**Slika 18.** Ukupna srednja vrijednost centričnosti testiranih instrumenata u zavijenim korijenskim kanalima

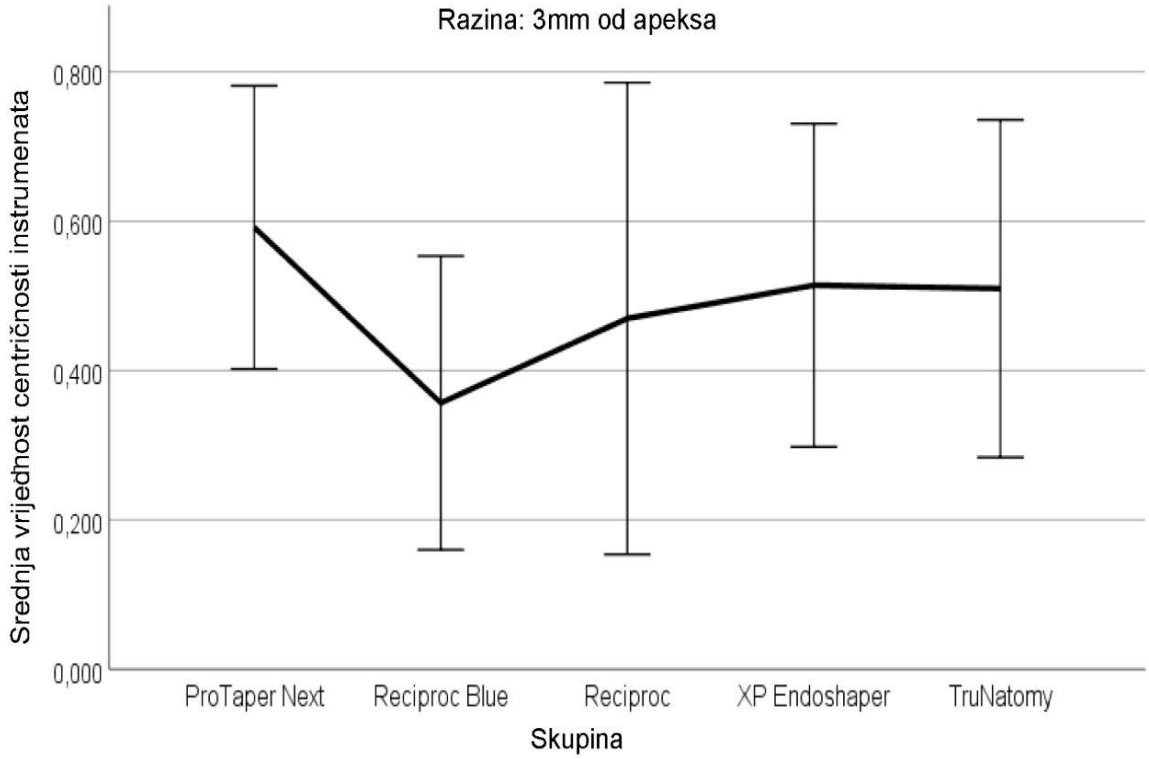
Na udaljenosti od 3 mm od apeksa nije bilo značajne razlike između pet testiranih tehnika u pogledu kanalne transportacije i centričnosti ($p > 0,05$) (Tablica 3, Slika 19, Slika 20) .

**Tablica 3.** Vrijednosti transportacije kanala i centričnosti na razini od 3 mm od apeksa s pet različitih tehnika instrumentacije

| **3mm** | | **N** | **Aritmetička sredina** | **SD** | **Standardna pogreška** | **95% interval pouzdanosti za aritmetičku sredinu** | | **Minimum** | **Maksimum** | **p** |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | | **Donja granica** | **Gornja granica** | | | |
| Transportacija kanala | ProTaper Next | 11 | 0,014 | 0,071 | 0,021 | -0,034 | 0,061 | -0,078 | 0,188 | 0,887 |
| | Reciproc Blue | 9 | -0,021 | 0,152 | 0,051 | -0,138 | 0,096 | -0,227 | 0,234 | |
| | Reciproc | 7 | 0,022 | 0,123 | 0,047 | -0,092 | 0,136 | -0,133 | 0,266 | |
| | XP Endoshaper | 9 | 0,009 | 0,073 | 0,024 | -0,047 | 0,065 | -0,100 | 0,150 | |
| | TruNatomy | 9 | 0,021 | 0,041 | 0,014 | -0,011 | 0,053 | -0,030 | 0,100 | |
| Centričnost instrumenta u kanalu | ProTaper Next | 11 | 0,592 | 0,282 | 0,085 | 0,402 | 0,781 | 0,300 | 1,000 | 0,502 |
| | Reciproc Blue | 9 | 0,357 | 0,256 | 0,085 | 0,160 | 0,553 | 0,096 | 0,813 | |
| | Reciproc | 7 | 0,470 | 0,342 | 0,129 | 0,154 | 0,786 | 0,158 | 0,871 | |
| | XP Endoshaper | 9 | 0,514 | 0,282 | 0,094 | 0,298 | 0,731 | 0,000 | 0,857 | |
| | TruNatomy | 9 | 0,510 | 0,294 | 0,098 | 0,284 | 0,736 | 0,000 | 1,000 | |




**Slika 19.** Transportacija kanala na razini od 3 mm od apeksa s pet različitih tehnika instrumentacije




**Slika 20.** Srednja vrijednost centričnosti instrumenta na razini 3 mm od apeksa

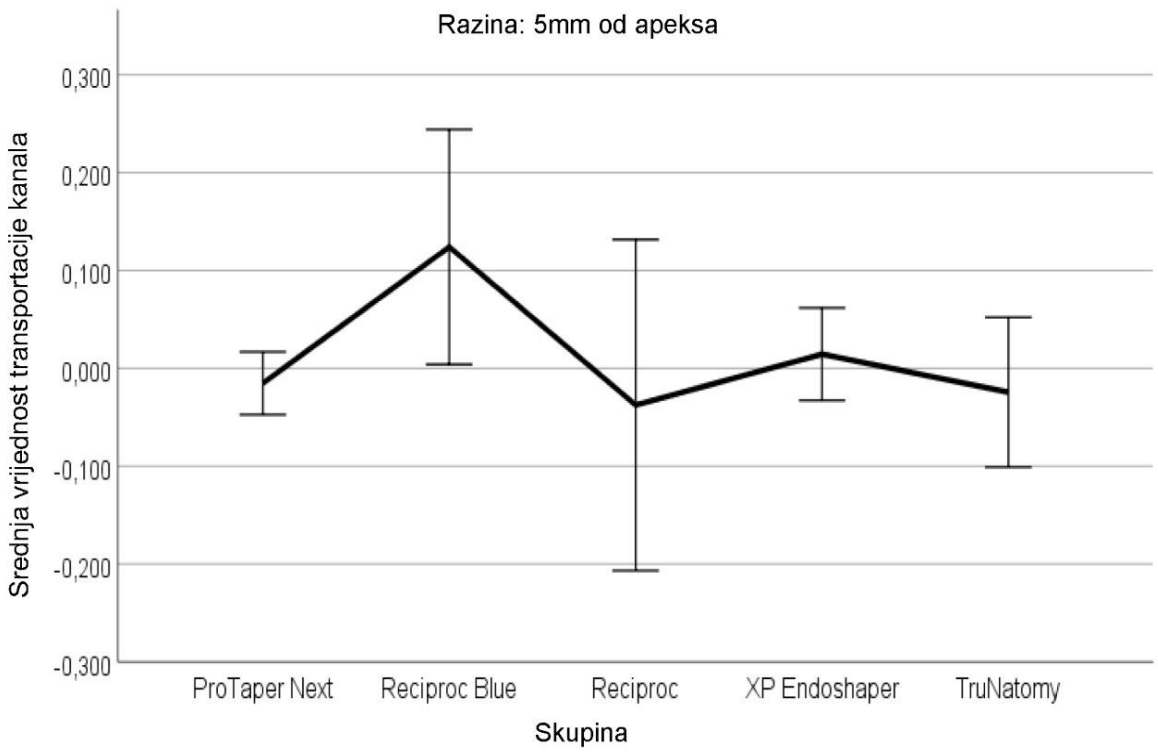
Na razini od 5 mm RCB je pokazao značajno veću kanalnu transportaciju nego PTN, RC, XPS i TRN ($p = 0,010$, $p = 0,008$, $p = 0,049$, $p = 0,009$).

Nije bilo razlika između tehnika PTN, RC, XPS i TRN u pogledu kanalne transportacije ($p = 0,730$) (Tablica 4, Slika 21).

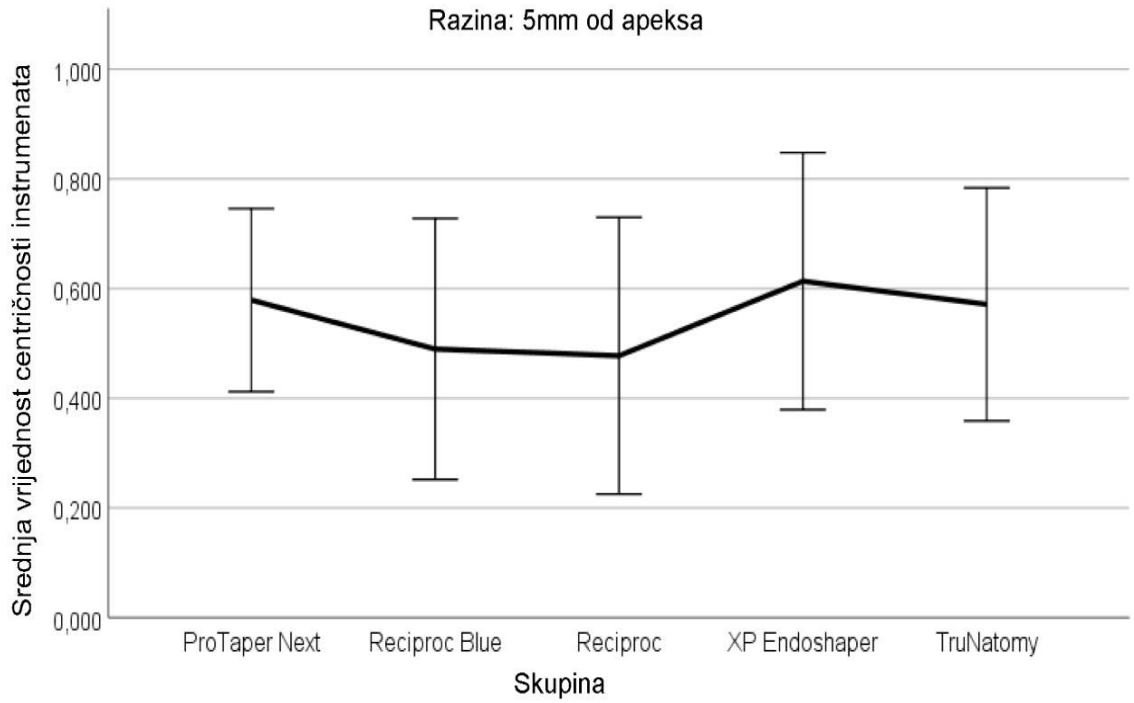
U analizi centričnosti instrumenta u kanalu testirane tehnike instrumentacije nisu pokazale značajnu razliku( $p > 0,05$) (Tablica 4, Slika 22).

**Tablica 4.** Vrijednosti transportacije kanala i centričnosti na razini od 5 mm od apeksa s pet različitih tehnika instrumentacije

| 5 mm | | N | Aritmetička sredina | SD | Standardna pogreška | 95% interval pouzdanosti za aritmetičku sredinu | | Minimum | Maksimum | p |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | | Donja granica | Gornja granica | | | |
| Transportacija kanala | ProTaper Next | 11 | -0,015 | 0,048 | 0,014 | -0,047 | 0,017 | -0,119 | 0,049 | 0,036 |
| | Reciproc Blue | 9 | 0,124 | 0,156 | 0,052 | 0,004 | 0,244 | -0,037 | 0,336 | |
| | Reciproc | 7 | -0,038 | 0,183 | 0,069 | -0,207 | 0,132 | -0,406 | 0,126 | |
| | XP Endoshaper | 9 | 0,014 | 0,061 | 0,020 | -0,033 | 0,062 | -0,110 | 0,090 | |
| | TruNatomy | 9 | -0,024 | 0,100 | 0,033 | -0,101 | 0,052 | -0,260 | 0,060 | |
| Centričnost instrumenta u kanalu | ProTaper Next | 11 | 0,579 | 0,249 | 0,075 | 0,412 | 0,746 | 0,190 | 1,000 | 0,826 |
| | Reciproc Blue | 9 | 0,490 | 0,310 | 0,103 | 0,252 | 0,728 | 0,178 | 0,939 | |
| | Reciproc | 7 | 0,478 | 0,273 | 0,103 | 0,225 | 0,730 | 0,086 | 0,840 | |
| | XP Endoshaper | 9 | 0,614 | 0,305 | 0,102 | 0,379 | 0,848 | 0,154 | 1,000 | |
| | TruNatomy | 9 | 0,571 | 0,276 | 0,092 | 0,359 | 0,784 | 0,212 | 1,000 | |




**Slika 21.** Transportacija kanala na razini od 5 mm od apeksa s pet različitih tehnika instrumentacije




**Slika 22.** Srednja vrijednost centričnosti testiranih instrumenata na razini od 5 mm od apeksa

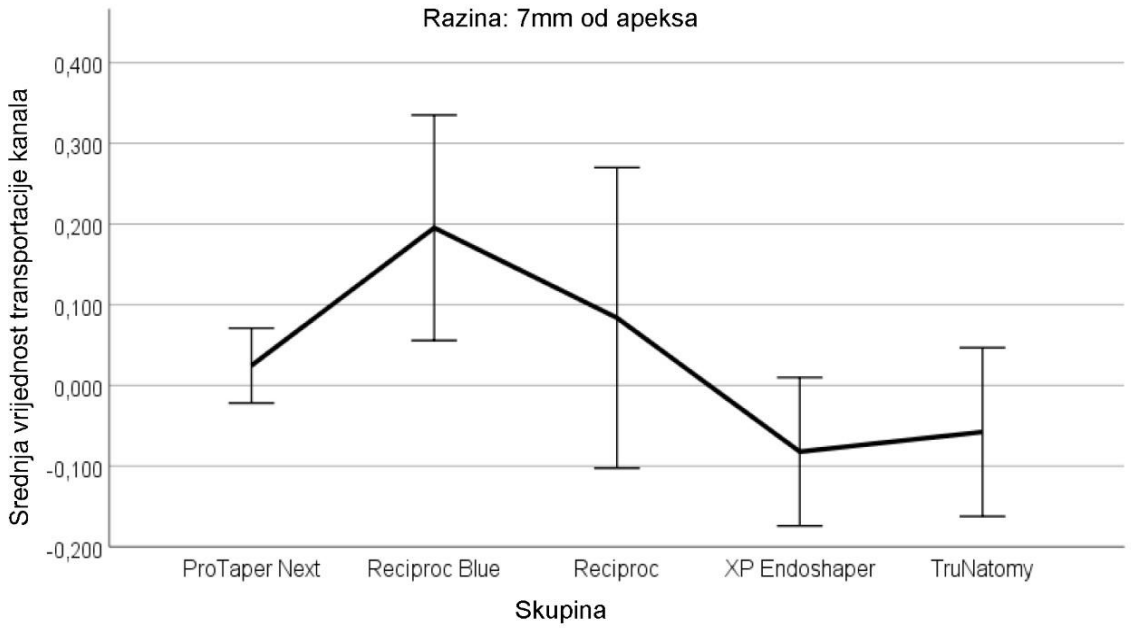
Na razini od 7 mm RCB je pokazao značajno veću kanalnu transportaciju nego PTN, XPS i TRN ($p = 0,011$, $p = 0,000$, $p = 0,001$), a u usporedbi s RC nije bilo značajne razlike ($p = 0,129$). Nije bilo značajne razlike između PTN, TRN i XPS ($p > 0,05$). PTN i TRN tehnike pokazale su sličnu kanalnu transportaciju kao RC tehnika ($p = 0,397$, $p = 0,057$). XPS je uzrokovao značajno manju transportaciju nego RC ($p = 0,027$) (Tablica 5, Slika 23).

Na razini od 7 mm od apeksa nije bilo značajne razlike u centričnosti između testiranih skupina ($p = 0,317$) (Tablica 5, Slika 24).

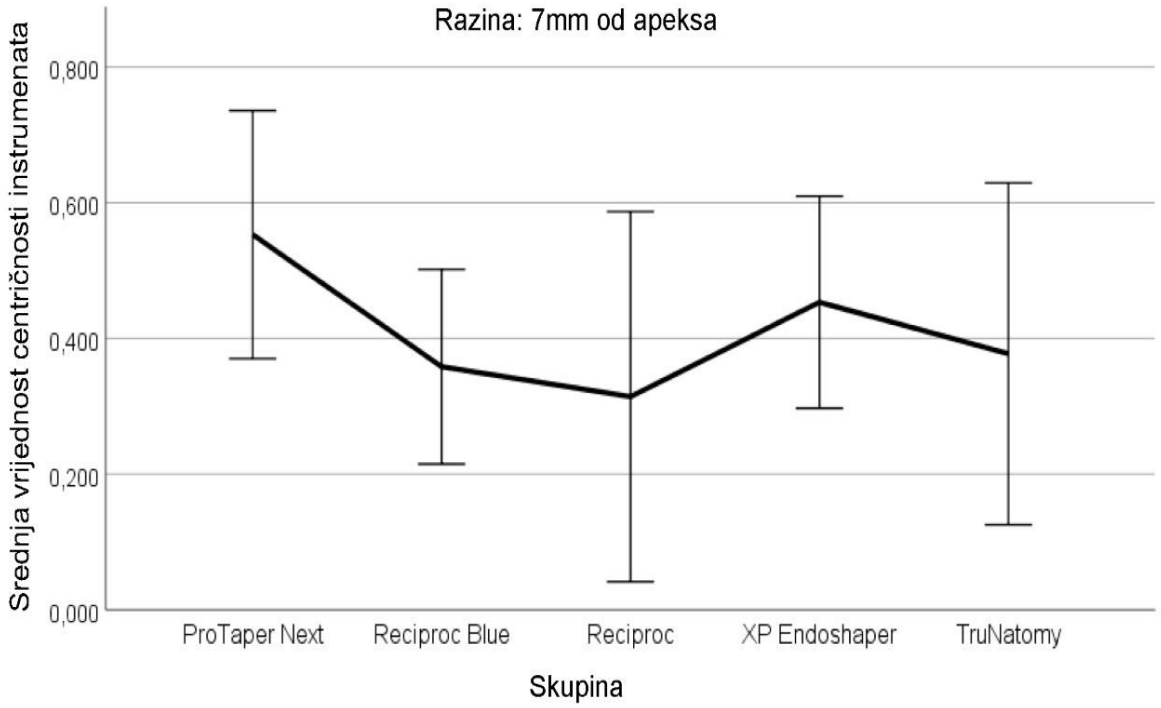
**Tablica 5.** Vrijednosti transportacije kanala i centričnosti na razini od 7 mm od apeksa s pet različitih tehnika instrumentacije

| 7mm | | N | Aritmetička sredina | SD | Standardna pogreška | 95% interval pouzdanosti za aritmetičku sredinu | | Minimum | Maksimum | P |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | | Donja granica | Gornja granica | | | |
| Transportacija kanala | ProTaper Next | 11 | 0,025 | 0,069 | 0,021 | -0,022 | 0,071 | -0,079 | 0,136 | 0,001 |
| | Reciproc Blue | 9 | 0,195 | 0,182 | 0,061 | 0,056 | 0,335 | -0,091 | 0,348 | |
| | Reciproc | 7 | 0,084 | 0,202 | 0,076 | -0,103 | 0,270 | -0,195 | 0,307 | |
| | XP Endoshaper | 9 | -0,082 | 0,120 | 0,040 | -0,174 | 0,010 | -0,330 | 0,050 | |
| | TruNatomy | 9 | -0,058 | 0,136 | 0,045 | -0,162 | 0,047 | -0,280 | 0,120 | |
| Centričnost instrumenta u kanalu | ProTaper Next | 11 | 0,553 | 0,272 | 0,082 | 0,370 | 0,736 | 0,142 | 0,849 | 0,317 |
| | Reciproc Blue | 9 | 0,358 | 0,187 | 0,062 | 0,215 | 0,502 | 0,193 | 0,633 | |
| | Reciproc | 7 | 0,314 | 0,295 | 0,111 | 0,041 | 0,587 | 0,097 | 0,849 | |
| | XP Endoshaper | 9 | 0,453 | 0,203 | 0,068 | 0,297 | 0,610 | 0,108 | 0,727 | |
| | TruNatomy | 9 | 0,377 | 0,328 | 0,109 | 0,125 | 0,629 | 0,034 | 1,000 | |

,




**Slika 23.** Transportacija kanala na razini od 7 mm od apeksa s pet različitih tehnika instrumentacije




**Slika 24.** Srednja vrijednost centričnosti instrumenta na razini od 7 mm od apeksa

# 5. RASPRAVA

Na tržištu se konstantno razvijaju nove tehnike instrumentacije radi jednostavnije mehaničke obrade korijenskih kanala, a da se pritom očuva njegov izvorni oblik bez nastanka proceduralnih pogrešaka (formiranje stepenice, blokada korijenskog kanala, prekomjerno stanjivanje kanalnih zidova, perforacija korijena zuba, lom instrumenta, apikalna transportacija). Zadržavanjem izvornog oblika kanala čuva se položaj apikalnog foramena i apikalni stop koji je bitan da ne bi dolazilo do instrumentacije preko radne duljine, protiskivanja nekrotičnog sadržaja i dentinske prašine/debrisa u periapikalni prostor. Uklanjanjem dentina tijekom instrumentacije slabi se korijen. Bitno je pratiti oblik/anatomiju kanala i ne proširivati kanal više nego što je potrebno kako bi se očuvao integritet zuba i što bolja funkcijska trajnost zuba. Ispravnom instrumentacijom dobiva se ljevkast oblik korijenskog kanala, što olakšava irigaciju i unošenje antibakterijskih intrakanalnih uložaka i materijala za punjenje korijenskih kanala (1).

Schilder je 1974. godine postavio principe oblikovanja korijenskih kanala po kojima:

1. kanal treba biti ljevkastog oblika, konstantnog koniciteta od apeksa do ulaza u korijenski kanal
2. poprečni presjek kanala treba se smanjivati prema apikalno
3. preparacija korijenskog kanala treba pratiti izvorni oblik kanala.
4. apikalni foramen treba zadržati svoj izvorni položaj
5. apikalni foramen treba održati što je moguće manjim.

Različiti postupci metalurške i termomehaničke obrade instrumenata rezultirali su povećanjem njihove fleksibilnosti i smanjenjem cikličkog te torzijskog zamora instrumenta (161, 162, 163, 164).

Rezultati našeg istraživanja pokazali su da rotacijske tehnike instrumentacije kanala, PTN, TRN i XPS, uzrokuju sličnu transportaciju kanala i imaju sličnu sposobnost centričmpsti instrumenta u zavijenim korijenskim kanalima na svim mjerenim razinama kanala (3 mm, 5 mm i 7 mm ). Transportacija kanala i sposobnost centričnosti instrumenta u kanalu mjerene su po Gambillu i suradnicima, kao što je već detaljno opisano u metodologiji. Ova se metoda koristi kao standard u većini radova na ovu temu (159).

Silva et al. (165) uspoređivali su ciklički i torzijski zamor novijih instrumenata zmijolikog oblika (XP-endo Shaper i TruShape). XP-endo Shaper pokazao je manji ciklički zamor nego

TruShape (P < 0,05). Autori navode da je razlog tome Max-wire Ni-Ti legura od koje se izrađuje XP-endo Shaper. Dodatni je čimbenik mali konicitet instrumenta XP-endo Shaper (0,01 inicijalni konicitet) u usporedbi s TruShape (0,06) i razlike u dizajnu poprečnog presjeka. Ova legura omogućava oblikovanje kanala koniciteta 0,04. Visoka otpornost na ciklički zamor XP-endo Shapera ukazuje na izrazitu fleksibilnost instrumenta. Zbog toga se pretpostavlja da su veoma sigurni i da uzrokuju manje neželjenih promjena u obliku korijenskog kanala tijekom instrumentacije zavijenih korijenskih kanala.

Sposobnost oblikovanja kanala pomoću različitih instrumentacijskih sustava detaljno je analizirana u brojnim istraživanjima u kojima su se pomoću mikro-CT-a analizirali različiti parametri: volumen uklonjenog dentina, povećanje intrakanalnog volumena, površina neinstrumentiranog intrakanalnog dentina, izravnavanje kanala, transportacija kanala, sposobnost centriranja instrumenta u kanalu (166, 167). Cilj svih tih istraživanja jest procijeniti mogu li i u kojoj mjeri broj instrumenata u određenom sistemu uz geometrijske, metalurške, dimenzijske te kinematičke razlike instrumenata i sistema instrumentacije utjecati na mehaničku obradu ravnih, zavijenih ili ovalnih kanala (167, 168, 169).

Stringheta i sur. (167) 2019. godine u svom su istraživanju analizirali volumen uklonjenog dentina, povećanje volumena kanala nakon preparacije, neinstrumentiranu površinu korijenskog kanala, volumen nakupljenog debrisa i strukturni model indeks (SMI) koristeći Reciproc, ProTaper Next, ProDesign Logic i WaveOne Gold. Ispitivani parametri uzeti su kao mjerilo kvalitete instrumentacije i čistoće kanala nakon preparacije (170, 171, 172). Nijedan sistem nije uspio dotaknuti sve stijenke korijenskog kanala i u potpunosti očistiti kanal. Slične rezultate dobili su i drugi istraživači. (172, 173, 174, 175, 176, 177). Ispitivani instrumenti dali su slične rezultate u svim parametrima osim za SMI, što za Stringhetu i sur. znači da nema značajnih razlika u kvaliteti instrumentacije ispitivanim instrumentima.

Arıcan Öztürk i sur. (168) 2020. godine ispitivali su i uspoređivali sposobnost oblikovanja kanala (engl. *shaping ability*) dviju tehnika XPS i PTN pomoću CBCT-a. Koristili su široke korijenske kanale jednokorijenskih zuba različitog promjera apikalno (#30, #35, #40) i promatrali promjene uzrokovane instrumentacijom u apikalnoj, srednjoj i koronarnoj trećini kanala. Ispitivane uzorke snimali su CBCT-om prije i nakon instrumentacije kako bi procijenili meziodistalnu i bukolingvalnu transportaciju kanala, centriranost instrumenta u kanalu, PA i PO na udaljenosti 2, 5 i 8 mm od apeksa. Ustanovili su da je učinkovitost ovih tehnika u

preparaciji jednokorijenskih zuba jednaka i da nema značajne razlike u transportaciji kanala i centriranosti instrumenta u kanalu.

XPS i TRN pripadaju novijim instrumentacijskim sustavima na tržištu. Karakterizira ih različita geometrija i veličina instrumenta, manje memorije oblika i jedinstvena metalurška obrada. Posebnu pažnju privukao je XPS kada ga je 2015. godine predstavila tvrtka FKG Dentaire (La Chaux-de-Fonds, Švicarska). Velozo i sur. (169) 2020. godine objavili su pregledni rad koji obuhvaća istraživanja XPS-a u obradi korijenskih kanala pomoću mikro-CT-a. Kao što mu i samo ime govori, XP-endo Shaper dizajniran je za oblikovanje korijenskog kanala. Instrument izvodi asimetričnu rotacijsku kretnju poprimajući polukružni, zmijoliki oblik, kada ekspandira na temperaturi od 35 °C ili većoj. Kada je na sobnoj temperaturi, instrument je u martenzičnoj fazi, a kada se unese u korijenski kanal, oblik mu se mijenja prelaskom u fazu austenita. Ovaj instrument ima i jedinstven vršak (engl. *booster tip*) sa šest reznih oštrica i početnim poprečnim presjekom ISO 15. U kanalu dolazi do ekspanzije instrumenta. Laganim pokretima i uz stalno ispiranje korijenskog kanala (nakon svakih pet laganih pokreta, prema uputama proizvođača) dostiže se završni oblik instrumentiranog kanala promjera ISO 30 na apeksu i koniciteta 0,04. XPS je proizveden od MaxWire legure (Martensite-Austenite Electropolishing-Flex, FKG), što mu omogućava bolju prilagodbu kanalnoj morfologiji dok se kontrahira i ekspandira napredujući do pune radne duljine (179, 180). Velozo i sur. (169) zaključili su da XP-endo Shaper daje dobre rezultate u oblikovanju korijenskih kanala, ali ne uspijeva dotaknuti sve zidove korijenskog kanala i u potpunosti očistiti intrakanalni prostor.

TRN je najnoviji rotirajući instrument tvrtke Dentsply Sirona predstavljen 2019. godine. Ovi instrumenti izrađuju se od Ni-Ti žice promjera 0,8 mm, koja podliježe posebnoj toplinskoj obradi, što rezultira superelastičnim svojstvima i manjom memorijom oblika. S obzirom na svoju geometriju regresivni konicitet (engl. *taper*) i uski dizajn, TRN osigurava poštednu, minimalno invazivnu preparaciju korijenskog kanala (181). TRN pokazuje i manji ciklički zamor u usporedbi s ProTaper Next (182).

Ponašanje PTN instrumenata u zavijenim korijenskim kanalima već je detaljno ispitano u prijašnjim istraživanjima koja su pokazala minimalnu transportaciju kanala. Transportacija je bila usporediva s ostalim rotacijskim tehnikama (166, 170, 183). Drukteinis i sur. (166) uspoređivali su učinkovitost PTN, BioRace i Genius instrumenata u oblikovanju zavijenih korijenskih kanala donjih prvih molara pomoću mikro-CT-a. Korijenske kanale instrumentirali

su *crown down* tehnikom do veličine ISO 35, koniciteta 0,04 za Bio Race i Genius grupe te do veličine ISO 30, koniciteta 0,07 za PTN grupu. Mikro-CT skenovi napravljeni su prije i nakon instrumentacije. Analizirali su promjene u volumenu dentina, postotak neinstrumentirane kanalne površine i transportaciju kanala u koronarnoj, srednjoj i apikalnoj trećini kanala. Ustanovili su da nema statistički značajne razlike između skupina za ispitivane parametre. Nije bilo značajne razlike u transportaciji kanala između tri navedene tehnike instrumentacije ni u jednoj kanalnoj trećini (P > 0,05).

Yilmaz i sur. (183) ispitivali su količinu uklonjenog dentina i transportaciju kanala nakon instrumentacije meziobukalnih kanala gornjih molara s PTN, One Shape i Edge File instrumentima pomoću mikro-CT-a. Količinu uklonjenog dentina mjerili su u koronarnoj trećini i čitavom dužinom kanala, a transportaciju kanala na udaljenosti 1 mm od apeksa. Nije uočena razlika među ispitivanim skupinama u količini uklonjenog dentina. Prosječna transportacija kanala u apikalnom je dijelu bila najmanja za PTN (0,197) (One Shape 0,263, Edge File 0,218) iako statistički značajne razlike nije bilo. Zaključili su da je količina uklonjenog dentina slična za sve tri ispitivane skupine i da nije bilo značajne transportacije kanala ni u jednom od ispitivanih sustava instrumentacije.

U usporedbi s recipročnim sustavom (Wave One) PTN uzrokuje znatno manji stupanj transportacije kanala i osigurava bolje centriranu preparaciju u apikalnom dijelu korijenskog kanala (184) (25). Štoviše, u našem istraživanju sekvenca instrumenata PTN X1 i PTNX2 rezultirala je najmanjom transportacijom kanala (0,008) i najbolje centriranom preparacijom (srednja vrijednost 0,510), ali ipak nije bila značajno superiornija naspram drugih testiranih rotacijskih tehnika (TRN, XPS). Prednosti PTN instrumenata u oblikovanju korijenskog kanala su: *off-centered* mali poprečni presjek koji je promjenjiv, progresivan konicitet u apikalnom dijelu koji se smanjuje u koronarnom dijelu instrumenta, što rezultira povećanom fleksibilnošću instrumenta i njegovom boljom prilagodbom u zavijenim korijenskim kanalima (95, 170, 184). Da Silva Limoeiro i sur. (170) uspoređivali su učinkovitost PTN i BioRace u instrumentaciji zavijenih korijenskih kanala pomoću mikro-CT-a. Nije bilo značajnih razlika među skupinama u količini uklonjenog dentina, transportaciji kanala i sposobnosti instrumenta da ostane centriran u kanalu. Zaključili su da su ove dvije tehnike instrumentacije jednako učinkovite.
U našem istraživanju XPS je uzrokovao značajno manju transportaciju u usporedbi s recipročnim sustavima (Reciproc i Reciproc Blue) na razini kanala od 5 mm (RCB) i 7 mm (RC i RCB). Slične rezultate objavili su Pacheco-Yanes i sur. (185) koji su također izmjerili manju

transporatciju XPS-a u usporedbi s RCB-om i RC-om i za apikalni dio kanala. Razlike u izmjerenim razlikama u transportaciji u apikalnom dijelu kanala mogle bi se objasniti razlikama u samoj metodologiji istraživanja. Naime Pacheco-Yanes et al. (185) u svom su istraživanju ispitivali instrumente u umjetnim kanalima izrađenim u blokovima od epoksi smole, što je moglo utjecati na konačan rezultat (160, 186). Ispitivanje instrumenata u prirodnom dentinu daje klinički pouzdanije rezultate (187). U drugom istraživanju Poly i sur. (188) XPS je uzrokovao manju transportaciju nego Wave One GOLD u zavijenim korijenskim kanalima. Autori su zaključili da je fleksibilnost legure XPS instrumenata djelomično odgovorna za bolju obradu kanala i bolje mehaničko ponašanje instrumenta u zavijenim kanalima (188). Ferandes i sur. (2020) (189) uspoređivali su instrumentaciju mezijalnih kanala mandibularnih molara pomoću Reciproca i XP-endo Shapera. Promatrali su promjene volumena kanala, postotak netaknutih zidova korijenskog kanala i volumen akumuliranog debrisa te devijaciju kanala u apikalnoj trećini. Zaključili su da je XP-Endo Shaper uspio dotaknuti značajno više kanalnih površina cijelom dužinom kanala, kao i u cervikalnoj i srednjoj trećini kada se analizira po trećinama. Ovi se rezultati povezuju sa svojstvima MaxWire legure koja instrumentu daje zmijoliki oblik na temperaturi iznad 35 ºC. Na toj temperaturi dolazi do promjene kristalne strukture iz faze martenzita u austenit. Ovo svojstvo legure povećava otpornost na trošenje instrumenta, što nije slučaj kod instrumenta kod kojih prevladava martenzična faza (3). Zmijoliki oblik instrumenta i ekscentrična rotacija omogućavaju veću kontaktnu površinu sa stijenkama dentina i osiguravaju bolji pristup teško dostupnim dijelovima kanala. U analizi apikalne trećine nije bilo značajnih razlika u netaknutim površinama kanala između analiziranih skupina. Uzrok tome je anatomija apikalnog dijela mezijalnih mandibularnih kanala koji su kružnog poprečnog presjeka, što limitira ekspanziju XPS-a.

Reciproc je uzrokovao značajno veću akumulaciju debrisa u čitavom kanalu, kao i u srednjoj i apikalnoj trećini. Nije bilo značajne razlike među skupinama u volumenu uklonjenog dentina (189).

Iako je XP-endo Shaper pokazao bolje rezultate u odnosu na rotirajuće tehnike u navedenim istraživanjima, potrebno je više studija da se razjasni moguća superiornost XPS-a nad recipročnim instrumentima u oblikovanju zavijenih korijenskih kanala.

U našem istraživanju XPS instrumenti uzrokovali su vrlo malu transportaciju kanala koja je bila usmjerena prema distalno (prosječna vrijednost -0,020). Slično je otkriveno i za TRN ( prosječna vrijednost -0,020). S druge strane ostale testirane tehnike uzrokovale su transportaciju kanala prema mezijalno. Također tehnike XPS i TRN imale su dobru sposobnost centriranja

instrumenta, ali bez značajnije superiornosti nad ostalim tehnikama. I u prethodnim istraživanjima dokazano je da novi sustav instrumentacije kanala, XPS, uzrokuje malu transportaciju kanala i dobru sposobnost centriranja instrumenta u zavijenim kanalima (32, 168, 188, 190).

Perez Moralez i sur. (32) ispitivali su sposobnost oblikovanja umjereno zakrivljenih kanala pomoću XPS-a i TruShape pomoću mikro-CT-a. U istraživanju su koristili maksilarne molare s dva korijenska kanala. Rezultati su pokazali da oba instrumenta uspijevaju očuvati izvornu anatomiju kanala, uzokuju malu/neznatnu transportaciju i da imaju dobru sposobnost centriranja u kanalu (32).

Najveći ukupni stupanj transportacije kanala u ovom istraživanju izmjeren je nakon primjene RCB instrumenta veličine 25 (srednja vrijednost 0,099). Ako pogledamo sve tri razine kanala (3 mm, 5 mm, 7 mm), RCB je uzrokovao najveću transportaciju na udaljenosti od 5 mm i 7 mm od apeksa u usporedbi s ostalim tehnikama. Slične rezultate objavili su Filizola de Oliveira i sur. (191) koji su uspoređivali ponašanje RCB, RC , PTN i TruShape instrumenata u zavijenim korijenskim kanalima mandibularnih molara. Analiza je izvršena pomoću mikro-CT-a. Zaključili su da instrumenti većeg koniciteta uzrokuju veće morfološke promjene kanala. Nije bilo značajne razlike ispitivanih sistema u dimenzijskim promjenama i apikalnoj transportaciji kanala neovisno o kinematici pokreta, broju instrumenata u sekvenci i vrsti toplinskog tretmana legure te pojedinačnim karakteristikama instrumenata (konicitet, dizajn) (191).

U obama istraživanjima izabrani instrumentacijski sustavi pokazali su sličnu transportaciju kanala i sposobnost centriranja instrumenta u apikalnom dijelu kanala. Ovi rezultati pokazuju da različit konicitet instrumenta, odnosno veći konicitet instrumenta na vrhu kod RCB i RC instrumenata (0,08) u usporedbi s PTN X2 (0,06) ne utječu na oblikovanje kanala u apikalnom dijelu (apikalna transportacija, centričnost instrumenta u kanalu). Razlog za ovakve rezultate u apikalnoj trećini za RC i RCB mogao bi biti prethodni rad instrumenta u cervikalnoj trećini kanala, što osigurava bolju centričnost instrumenta i njegov direktan pristup u apikalni dio kanala (192, 193). U srednjoj trećini kanala RCB je pokazao veću transportaciju nego ostale tehnike, što je vjerojatno uzrokovano smanjenjem memorije RCB-a (100). Nadalje neka istraživanja pokazala su da uvođenje prethodno zavijenih instrumenata u kanal može uzrokovati veću kanalnu transportaciju u srednjoj trećini (194, 195), što bi također moglo objasniti rezultate ovog istraživanja. Konačno, neki autori (188) navode da recipročni sistemi

uzrokuju veće nakupljanje debrisa na zidovima kanalnog dentina, što također može utjecati na kanalnu transportaciju.

Zanimljivo otkriće ovog istraživanja je veća transportacija kanala RCB instrumentom od RC instrumenta na razini kanala od 5 mm. Geometrija i kinematika obaju sistema je ista. Jedina razlika je toplinska obrada RCB-a, koja osigurava veću fleksibilnost i manji ciklički zamor instrumenta (164, 196). Razlike između RC i RCB instrumenata u ovom istraživanju mogle bi se objasniti s nekoliko razloga pronađenih u objavljenoj literaturi. Filizola de Oliveira i sur. (191) u već spomenutom istraživanju dobili su veću transportaciju kanala u srednjoj trećini s RCB instrumentima nego s PTN-om i TRU-om. Ovu razliku objasnili su smanjenjem memorije obilka RCB-a. Smanjena memorija oblika omogućava uvođenje prethodno zavijenog instrumenta u kanal (100). Slična istraživanja pokazala su da uvođenje prethodno zavijenih instrumenata u kanal može uzrokovati veću transportaciju u srednjoj trećini korijenskog kanala (194, 195). Nadalje Bürklein et al. (197) otkrili su da plava toplinska obrada instrumenta ne rezultira nižim vrijednostima transportacije. Također se nagađa da površinska termička obrada RCB-a čini instrument tvrđim nego neobrađeni Ni-Ti instrument i najmanje pet puta tvrđim od dentina (188, 198). Međutim u literaturi ne postoje jasni rezultati koji potkrepljuju ove pretpostavke (188). Prema našim saznanjima dosad je objavljeno svega nekoliko istraživanja koja su uspoređivala RCB i RC instrumente u nastanku transportacije kanala (191, 199). U objema navedenim studijama instrumenti RCB i RC pokazali su sličnu kanalnu transportaciju. Uspoređujući metodologije navedenih istraživanja s našom uočena je razlika u istraživanju Belladonna i sur. (199) u stupnju zavijenosti korijenskih kanala, što bi potencijalno moglo utjecati na stupanj kanalne transportacije.

Belladona i sur. (199) na mezijalnim su korijenima donjih prvih i drugih molara srednje zavijenosti ispitivali učinkovitost oblikovanja kanala s Reciproc i Reciproc Blue. Reciproc i RCB pokazali su sličnu transportaciju kanala na svim razinama kanala. Autori to objašnjavaju dizajnom ovih instrumenata. Oba instrumenta imaju nerežući brid koji olakšava prodiranje instrumenta u kanal uz minimalan pritisak. Iako su očekivali da će poboljšana svojstva Reciproc Blue dati manje vrijednosti transportacije kanala, ispostavilo se da je Reciproc jednako učinkovit u obradi korijenskih kanala.

Rezultati našeg istraživanja mogu se kritički analizirati iz perspektive kliničkog značaja. Wu i sur. (200) zaključili su da apikalna transportacija manja od 0,3 mm ima minimalan utjecaj na prognozu liječenja. U našem istraživanju kanalna transportacija bila je manja od 0,3 mm u svim

razinama korijenskog kanala i za sve testirane tehnike instrumentacije. Iako je postojala značajna razlika u transportaciji između grupa na razini od 5 mm i 7 mm na srednjoj trećini korijenskih kanala, ova razlika prema Wu i sur. nema klinički značaj (200).

# 6. ZAKLJUČAK

1. Tehnika Reciproc Blue uzrokovala je veću transportaciju zavijenih kanala od rotacijskih tehnika, ProTaper Next, TruNatomy i XP-EndoShaper, koje su pokazale sličnu i malu transportaciju kanala.
2. U apikalnoj trećini kanala, sve testirane tehnike pokazale su malu i sličnu transportaciju kanala, dok je u srednjoj i cervikalnoj trećini Reciproc Blue tehnika uzrokovala najveću transportaciju kanala.
3. Analiza centričnosti instrumenta unutar cijelog kanala pokazala je da ProTaper Next tehnika ima najveću sposobnost da ostane centrirana unutar zavijenog kanala tijekom instrumentacije.
4. U apikalnoj trećini, sve testirane tehnike pokazale su sličnu centričnost.

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# 8. ŽIVOTOPIS

Emina Kabil rođena je 31. kolovoza 1989. godine u Tuzli (Bosna i Hercegovina). Osnovnu školu, srednju glazbenu školu i Gimnaziju "Meša Selimović" završila je u Tuzli. Na Stomatološki fakultet Sveučilišta u Zagrebu upisala se 2008. godine. Tijekom studija bila je aktivna u Udruzi studenata dentalne medicine i u Europskoj udruzi studenata dentalne medicine (u kojoj je akademske godine 2012./2013. bila koordinatorica za međunarodne razmjene studenata u Europi, a 2013. /2014. godine glavna urednica časopisa Europske udruge studenata dentalne medicine).

Dobitnica je posebne Rektorove nagrade za Geronto projekt – Evaluacija i unapređenje oralnog zdravlja u osoba starije životne dobi u akademskoj godini 2012./2013.

Sudjelovala je u istraživačkom projektu "Stem cells in dental medicine" na King's College u Londonu u kolovozu 2012. godine.

Diplomirala je na Stomatološkom fakultetu 2014. godine. Od listopada 2014. do ožujka 2015. godine stažirala je u Domu zdravlja Zagreb zapad. Od studenog 2015. do ljeta 2017. godine radila je kao znanstveni novak na Privatnom stomatološkom fakultetu u Kremsu (Danube Private University) na Zavodu za endodonciju, restaurativnu stomatologiju i parodontologiju. Od ljeta 2017. godine radi u privatnoj stomatološkoj ordinaciji Zahnärzte am Karlsplatz u Beču. Godine 2019. apsolvirala je Curriculum iz endodoncije u Beču. Uz materinji jezik tečno govori engleski i njemački jezik. Članica je Hrvatskog endodontskog društva, Austrijskog endodontskog društva, Austrijske stomatološke komore i Europskog društva za endodonciju (ESE).

Objavljeni radovi:

- Kabil E, Katić M, Anić I, Bago I. Micro-computed Evaluation of Canal Transportation and Centering Ability of 5 Rotary and Reciprocating Systems with Different Metallurgical Properties and Surface Treatments in Curved Root Canals. J Endod. 2021;47(3): 477 - 84. (**Rad proizašao iz doktorata**, IF 2,886, Q1 prema WoS i Scopusu)
- Antunović M, Vukmanović Lj, Budimir A, Kabil E, Anić I, Bago I. Evaluation of Sealing Ability of Four Bioceramic Root Canal Sealers and an Epoxy Resin-based Sealer: An *in vitro* study. Saudi Endod J. 2021,11: 66 - 72. (IF 1,94, Q3 prema WoS i Scopusu)

# Preflight Results

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